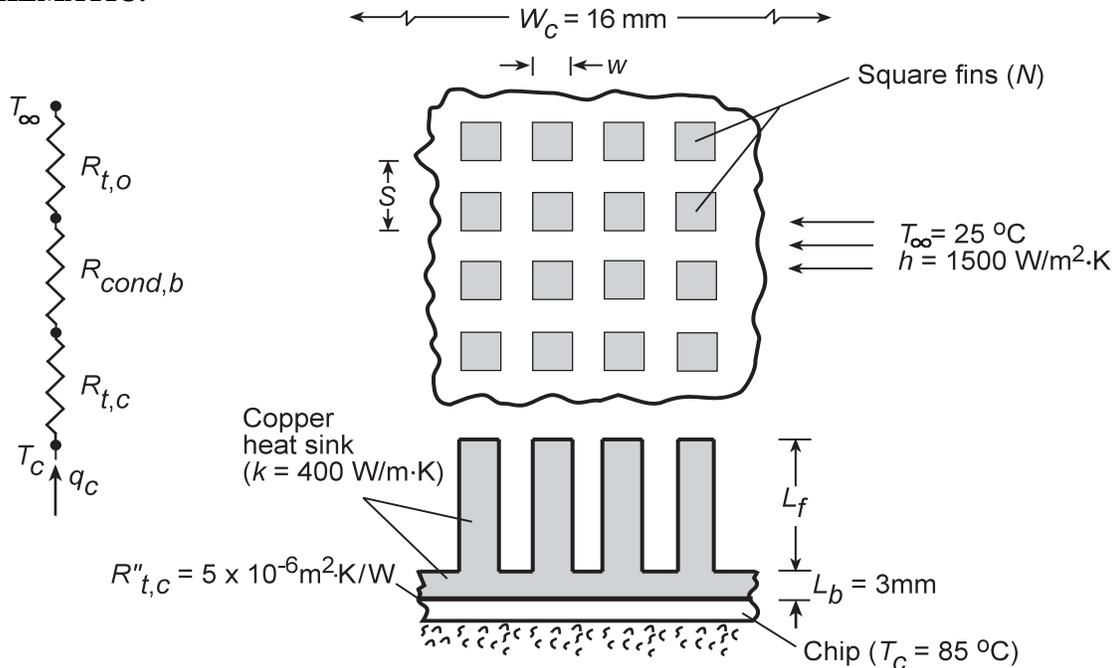


### PROBLEM 3.150

**KNOWN:** Copper heat sink dimensions and convection conditions.

**FIND:** (a) Maximum allowable heat dissipation for a prescribed chip temperature and interfacial chip/heat-sink contact resistance, (b) Effect of fin length and width on heat dissipation.

**SCHEMATIC:**



**ASSUMPTIONS:** (1) Steady-state conditions, (2) One-dimensional heat transfer in chip-heat sink assembly, (3) Constant  $k$ , (4) Negligible chip thermal resistance, (5) Negligible heat transfer from back of chip, (6) Uniform chip temperature.

**ANALYSIS:** (a) For the prescribed system, the chip power dissipation may be expressed as

$$q_c = \frac{T_c - T_\infty}{R_{t,c} + R_{\text{cond},b} + R_{t,o}}$$

where  $R_{t,c} = \frac{R''_{t,c}}{W_c^2} = \frac{5 \times 10^{-6} \text{ m}^2 \cdot \text{K}/\text{W}}{(0.016 \text{ m})^2} = 0.0195 \text{ K}/\text{W}$

$$R_{\text{cond},b} = \frac{L_b}{kW_c^2} = \frac{0.003 \text{ m}}{400 \text{ W}/\text{m} \cdot \text{K} (0.016 \text{ m})^2} = 0.0293 \text{ K}/\text{W}$$

The thermal resistance of the fin array is

$$R_{t,o} = (\eta_o h A_t)^{-1}$$

where  $\eta_o = 1 - \frac{N A_f}{A_t} (1 - \eta_f)$

and  $A_t = N A_f + A_b = N(4wL_c) + (W_c^2 - Nw^2)$

Continued...

### PROBLEM 3.150 (Cont.)

With  $w = 0.25$  mm,  $S = 0.50$  mm,  $L_f = 6$  mm,  $N = 1024$ , and  $L_c \approx L_f + w/4 = 6.063 \times 10^{-3}$  m, it follows that  $A_f = 6.06 \times 10^{-6}$  m<sup>2</sup> and  $A_t = 6.40 \times 10^{-3}$  m<sup>2</sup>. The fin efficiency is

$$\eta_f = \frac{\tanh mL_c}{mL_c}$$

where  $m = (hP/kA_c)^{1/2} = (4h/kw)^{1/2} = 245$  m<sup>-1</sup> and  $mL_c = 1.49$ . It follows that  $\eta_f = 0.608$  and  $\eta_o = 0.619$ , in which case

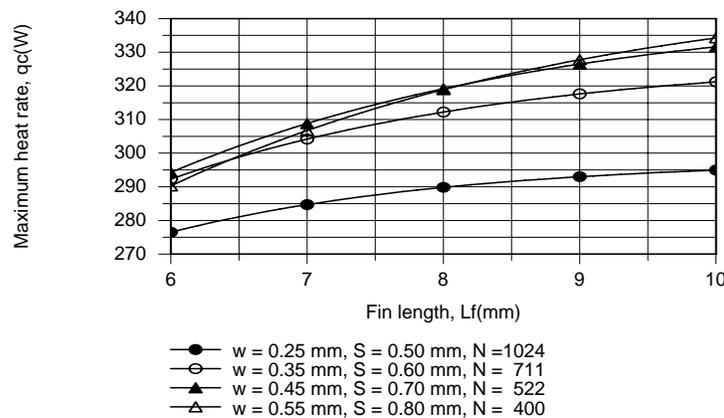
$$R_{t,o} = \left( 0.619 \times 1500 \text{ W/m}^2 \cdot \text{K} \times 6.40 \times 10^{-3} \text{ m}^2 \right) = 0.168 \text{ K/W}$$

and the maximum allowable heat dissipation is

$$q_c = \frac{(85 - 25)^\circ \text{C}}{(0.0195 + 0.0293 + 0.168) \text{ K/W}} = 276 \text{ W}$$

(b) The IHT *Performance Calculation, Extended Surface Model* for the *Pin Fin Array* has been used to determine  $q_c$  as a function of  $L_f$  for four different cases, each of which is characterized by the closest allowable fin spacing of  $(S - w) = 0.25$  mm.

Case	w (mm)	S (mm)	N
A	0.25	0.50	1024
B	0.35	0.60	711
C	0.45	0.70	522
D	0.55	0.80	400



With increasing  $w$  and hence decreasing  $N$ , there is a reduction in the total area  $A_t$  associated with heat transfer from the fin array. However, for Cases A through C, the reduction in  $A_t$  is more than balanced by an increase in  $\eta_f$  (and  $\eta_o$ ), causing a reduction in  $R_{t,o}$  and hence an increase in  $q_c$ . As the fin efficiency approaches its limiting value of  $\eta_f = 1$ , reductions in  $A_t$  due to increasing  $w$  are no longer balanced by increases in  $\eta_f$ , and  $q_c$  begins to decrease. Hence there is an optimum value of  $w$ , which depends on  $L_f$ . For the conditions of this problem,  $L_f = 10$  mm and  $w = 0.55$  mm provide the largest heat dissipation.