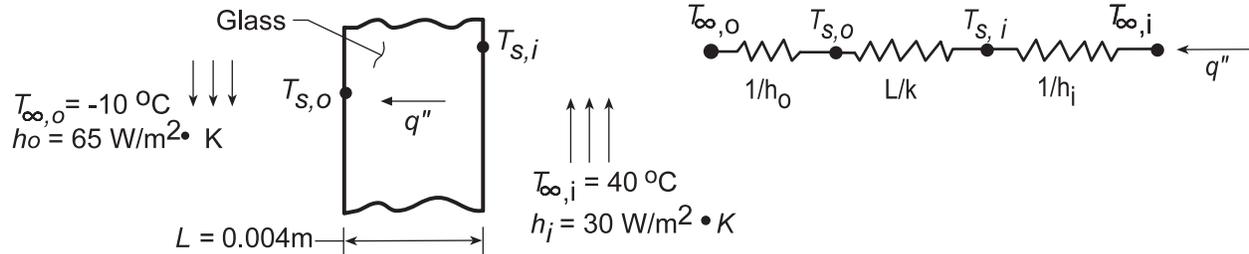


PROBLEM 3.3

KNOWN: Temperatures and convection coefficients associated with air at the inner and outer surfaces of a rear window.

FIND: (a) Inner and outer window surface temperatures, $T_{s,i}$ and $T_{s,o}$, and (b) $T_{s,i}$ and $T_{s,o}$ as a function of the outside air temperature $T_{\infty,o}$ and for selected values of outer convection coefficient, h_o .

SCHEMATIC:



ASSUMPTIONS: (1) Steady-state conditions, (2) One-dimensional conduction, (3) Negligible radiation effects, (4) Constant properties.

PROPERTIES: Table A-3, Glass (300 K): $k = 1.4 \text{ W/m}\cdot\text{K}$.

ANALYSIS: (a) The heat flux may be obtained from Eqs. 3.11 and 3.12,

$$q'' = \frac{T_{\infty,i} - T_{\infty,o}}{\frac{1}{h_o} + \frac{L}{k} + \frac{1}{h_i}} = \frac{40^\circ\text{C} - (-10^\circ\text{C})}{\frac{1}{65 \text{ W/m}^2 \cdot \text{K}} + \frac{0.004 \text{ m}}{1.4 \text{ W/m}\cdot\text{K}} + \frac{1}{30 \text{ W/m}^2 \cdot \text{K}}}$$

$$q'' = \frac{50^\circ\text{C}}{(0.0154 + 0.0029 + 0.0333) \text{ m}^2 \cdot \text{K/W}} = 969 \text{ W/m}^2.$$

Hence, with $q'' = h_i (T_{\infty,i} - T_{s,o})$, the inner surface temperature is

$$T_{s,i} = T_{\infty,i} - \frac{q''}{h_i} = 40^\circ\text{C} - \frac{969 \text{ W/m}^2}{30 \text{ W/m}^2 \cdot \text{K}} = 7.7^\circ\text{C} \quad <$$

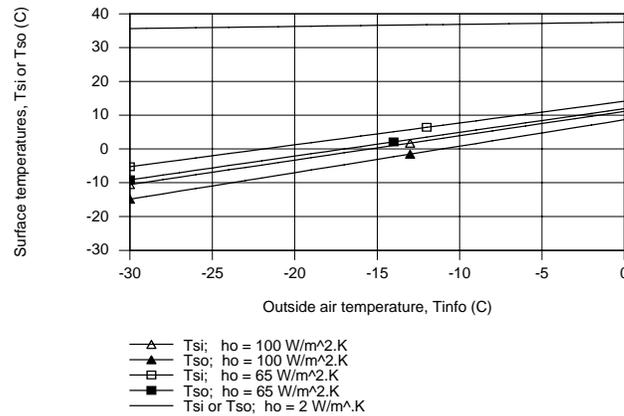
Similarly for the outer surface temperature with $q'' = h_o (T_{s,o} - T_{\infty,o})$ find

$$T_{s,o} = T_{\infty,o} + \frac{q''}{h_o} = -10^\circ\text{C} + \frac{969 \text{ W/m}^2}{65 \text{ W/m}^2 \cdot \text{K}} = 4.9^\circ\text{C} \quad <$$

(b) Using the same analysis, $T_{s,i}$ and $T_{s,o}$ have been computed and plotted as a function of the outside air temperature, $T_{\infty,o}$, for outer convection coefficients of $h_o = 2, 65, \text{ and } 100 \text{ W/m}^2\cdot\text{K}$. As expected, $T_{s,i}$ and $T_{s,o}$ are linear with changes in the outside air temperature. The difference between $T_{s,i}$ and $T_{s,o}$ increases with increasing convection coefficient, since the heat flux through the window likewise increases. This difference is larger at lower outside air temperatures for the same reason. Note that with $h_o = 2 \text{ W/m}^2\cdot\text{K}$, $T_{s,i} - T_{s,o}$, is too small to show on the plot.

Continued ...

PROBLEM 3.3 (Cont.)

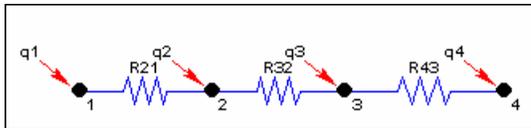


COMMENTS: (1) The largest resistance is that associated with convection at the inner surface. The values of $T_{s,i}$ and $T_{s,o}$ could be increased by increasing the value of h_i .

(2) The *IHT Thermal Resistance Network Model* was used to create a model of the window and generate the above plot. The Workspace is shown below.

// Thermal Resistance Network Model:

// The Network:



// Heat rates into node j , q_j , through thermal resistance R_{ij}

$$q_{21} = (T_2 - T_1) / R_{21}$$

$$q_{32} = (T_3 - T_2) / R_{32}$$

$$q_{43} = (T_4 - T_3) / R_{43}$$

// Nodal energy balances

$$q_1 + q_{21} = 0$$

$$q_2 - q_{21} + q_{32} = 0$$

$$q_3 - q_{32} + q_{43} = 0$$

$$q_4 - q_{43} = 0$$

/* Assigned variables list: deselect the q_j , R_{ij} and T_i which are unknowns; set $q_i = 0$ for embedded nodal points at which there is no external source of heat. */

$T_1 = T_{info}$ // Outside air temperature, C

// $q_1 =$ // Heat rate, W

$T_2 = T_{so}$ // Outer surface temperature, C

$q_2 = 0$ // Heat rate, W; node 2, no external heat source

$T_3 = T_{si}$ // Inner surface temperature, C

$q_3 = 0$ // Heat rate, W; node 3, no external heat source

$T_4 = T_{infi}$ // Inside air temperature, C

// $q_4 =$ // Heat rate, W

// Thermal Resistances:

$R_{21} = 1 / (h_o * A_s)$ // Convection thermal resistance, K/W; outer surface

$R_{32} = L / (k * A_s)$ // Conduction thermal resistance, K/W; glass

$R_{43} = 1 / (h_i * A_s)$ // Convection thermal resistance, K/W; inner surface

// Other Assigned Variables:

$T_{info} = -10$ // Outside air temperature, C

$h_o = 65$ // Convection coefficient, $W/m^2.K$; outer surface

$L = 0.004$ // Thickness, m; glass

$k = 1.4$ // Thermal conductivity, $W/m.K$; glass

$T_{infi} = 40$ // Inside air temperature, C

$h_i = 30$ // Convection coefficient, $W/m^2.K$; inner surface

$A_s = 1$ // Cross-sectional area, m^2 ; unit area