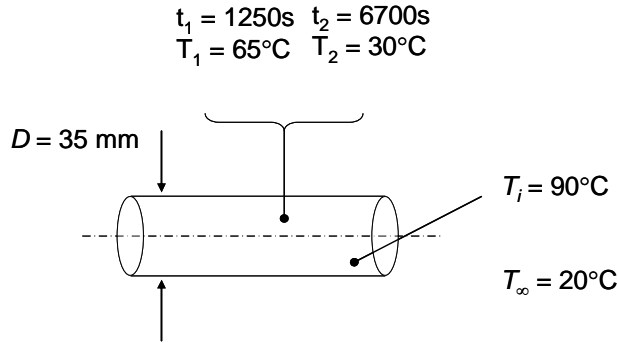


### PROBLEM 5.38

**KNOWN:** Diameter of highly polished aluminum rod. Temperature of rod initially and at two later times. Room air temperature.

**FIND:** Values of constants  $C$  and  $n$  in Equation 5.26. Plot rod temperature vs. time for varying and constant heat transfer coefficients.

**SCHEMATIC:**



**ASSUMPTIONS:** (1) Constant properties, (2) Radiation negligible because rod is highly polished, (3) Lumped capacitance approximation is valid.

**PROPERTIES:** Table A.1, Aluminum ( $T = 328$  K):  $c = 916$  J/kg·K,  $\rho = 2702$  kg/m<sup>3</sup>,  $k = 238$  W/m·K.

**ANALYSIS:** If the heat transfer coefficient is given by Equation 5.26, then the temperature as a function of time is given by Equation 5.28:

$$\frac{\theta}{\theta_i} = \left[ \frac{nCA_{s,c}\theta_i^n}{\rho Vc} t + 1 \right]^{-1/n} \quad (1)$$

where  $\theta = T - T_\infty$  and  $A_{s,c}$  is the area exposed to convection,  $A_{s,c} = \pi DL$ . Since the rod temperature is known at two different times, Equation (1) can be evaluated at these two times, making it possible to solve for the two unknowns,  $C$  and  $n$ . The two equations are

$$\frac{\theta_1}{\theta_i} = \left[ \frac{nCA_{s,c}\theta_i^n}{\rho Vc} t_1 + 1 \right]^{-1/n} \quad \frac{\theta_2}{\theta_i} = \left[ \frac{nCA_{s,c}\theta_i^n}{\rho Vc} t_2 + 1 \right]^{-1/n} \quad (2a,b)$$

These equations cannot be explicitly solved for  $C$  and  $n$ . They can be numerically solved in this form, using IHT or some other software, or they can be further manipulated to solve for the times:

$$t_1 = \left[ \left( \frac{\theta_1}{\theta_i} \right)^{-n} - 1 \right] \frac{\rho c D}{4n C \theta_i^n} \quad t_2 = \left[ \left( \frac{\theta_2}{\theta_i} \right)^{-n} - 1 \right] \frac{\rho c D}{4n C \theta_i^n} \quad (3a,b)$$

where we have used  $V/A_{s,c} = D/4$ . Taking the ratio of Equations (3a) and (3b) yields

$$\frac{t_2}{t_1} = \frac{\left( \frac{\theta_2}{\theta_i} \right)^{-n} - 1}{\left( \frac{\theta_1}{\theta_i} \right)^{-n} - 1} = \frac{6700 \text{ s}}{1250 \text{ s}} = \frac{\left( \frac{30^\circ\text{C} - 20^\circ\text{C}}{90^\circ\text{C} - 20^\circ\text{C}} \right)^{-n} - 1}{\left( \frac{65^\circ\text{C} - 20^\circ\text{C}}{90^\circ\text{C} - 20^\circ\text{C}} \right)^{-n} - 1} \quad 5.36 = \frac{(0.143)^{-n} - 1}{(0.643)^{-n} - 1} \quad (4a,b,c)$$

Continued...

### PROBLEM 5.38 (Cont.)

This can be iteratively or numerical solved for  $n$ , to find  $n = 0.25$ . Then  $C$  can be determined from Equation (3a) or (3b):

$$C = \left[ \left( \frac{\theta_1}{\theta_i} \right)^{-n} - 1 \right] \frac{\rho c D}{4n\theta_i^n t_1} = \left[ \left( \frac{45^\circ\text{C}}{70^\circ\text{C}} \right)^{-0.25} - 1 \right] \frac{2702 \text{ kg/m}^3 \times 916 \text{ J/kg} \cdot \text{K} \times 0.035 \text{ m}}{4 \times 0.25 \times (70^\circ\text{C})^{0.25} \times 1250 \text{ s}} = 2.8 \text{ W/m}^2 \cdot \text{K}^{1.25}$$

$$C = 2.8 \text{ W/m}^2 \cdot \text{K}^{1.25}, n = 0.25$$

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Now that these constants are known, the validity of the lumped capacitance approximation can be checked. The maximum heat transfer coefficient occurs at the initial time,

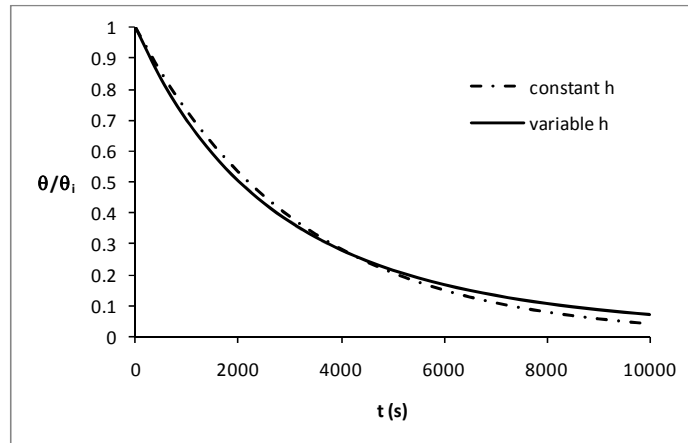
$$h = C(T - T_\infty)^n = 2.8 \text{ W/m}^2 \cdot \text{K}^{1.25} [(90 - 20)\text{K}]^{0.25} = 8.1 \text{ W/m}^2 \cdot \text{K}$$

Thus, using the conservative definition,  $Bi = hD/2k = 6 \times 10^{-4}$ . The lumped capacitance approximation is valid.

The heat transfer coefficient corresponding to a rod temperature of  $\bar{T} = (T_i + T_\infty)/2 = 55^\circ\text{C}$  is

$$h = C(T - T_\infty)^n = 2.8 \text{ W/m}^2 \cdot \text{K}^{1.25} [(55 - 20)\text{K}]^{0.25} = 6.8 \text{ W/m}^2 \cdot \text{K}$$

The plot below shows the rod temperature as a function of time using Equation (1) above for variable heat transfer coefficient, as well as the rod temperature assuming the constant value of  $h = 6.8 \text{ W/m}^2 \cdot \text{K}$ , using text Equation 5.6.



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**COMMENTS:** (1) Since the heat transfer coefficient is temperature difference-dependent (variable  $h$ ), the initial cooling rates are larger when this dependence is accounted for. As the temperature difference decreases, the variable  $h$  case cools slower relative to the constant  $h$  case. (2) The discrepancy between the variable and constant heat transfer coefficient cases is not large under these conditions. The difference would be greater if  $n$  were larger.