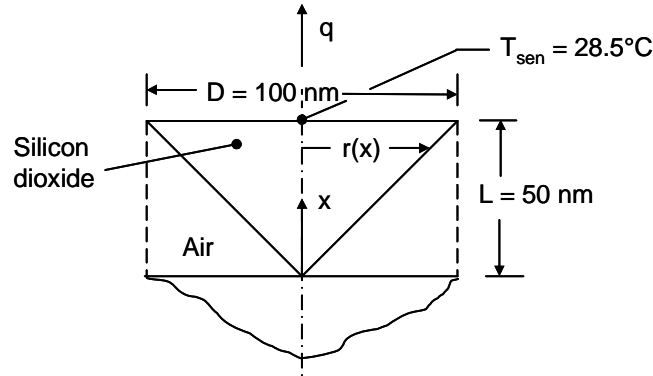


### PROBLEM 3.44

**KNOWN:** Construction and dimensions of a device to measure the temperature of a surface. Ambient and sensing temperatures, and thermal resistance between the sensing element and the pivot point.

**FIND:** (a) Thermal resistance between the surface temperature and the sensing temperature, (b) Surface temperature for  $T_{\text{sen}} = 28.5^\circ\text{C}$ .

**SCHEMATIC:**



**ASSUMPTIONS:** (1) Steady-state conditions, (2) One-dimensional heat transfer, (3) Negligible nanoscale effects, (4) Constant properties.

**PROPERTIES:** Table A.2, polycrystalline silicon dioxide (300 K):  $k = 1.38 \text{ W/m}\cdot\text{K}$ . Table A.4, air (300 K):  $k = 0.0263 \text{ W/m}\cdot\text{K}$ .

**ANALYSIS:**

(a) At any  $x$  location, heat transfer in the  $x$ -direction occurs by conduction in the air as well as conduction in the probe. Applying Fourier's law,

$$q_x = -k_a A_a \frac{dT}{dx} - k_p A_p \frac{dT}{dx} \quad (1)$$

Since the probe radius is  $r = Dx/2L$ , the probe area is

$$A_p = \frac{\pi D^2}{4L^2} x^2 \quad \text{and} \quad A_a = \frac{\pi D^2}{4} - A_p = \frac{\pi D^2}{4} \left[ 1 - \frac{x^2}{L^2} \right] \quad (2a, 2b)$$

Substituting Eqs. (2a) and (2b) into Eq. (1) yields

$$q_x = -\frac{\pi D^2}{4L^2} \left[ k_a (L^2 - x^2) + k_p x^2 \right] \frac{dT}{dx}$$

Separating variables and integrating,

Continued...

### PROBLEM 3.44 (Cont.)

$$q_x \int_{x=0}^L \frac{dx}{k_a(L^2 - x^2) + k_p x^2} = - \frac{\pi D^2}{4L^2} \int_{T=T_{\text{surf}}}^{T_{\text{sen}}} dT = - \frac{\pi D^2}{4L^2} (T_{\text{sen}} - T_{\text{surf}})$$

Therefore, the thermal resistance associated with the probe is

$$R_{\text{sen}} = \frac{(T_{\text{surf}} - T_{\text{sen}})}{q_x} = \frac{4L^2}{\pi D^2} \int_{x=0}^L \frac{dx}{k_a L^2 + (k_p - k_a)x^2}$$

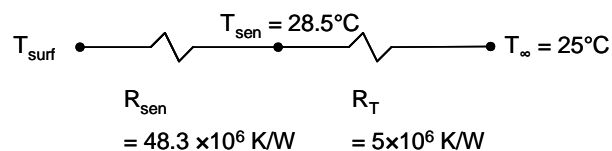
Carrying out the integration yields

$$R_{\text{sen}} = \frac{4L^2}{\pi D^2} \frac{1}{\sqrt{k_a(k_p - k_a)}} \tan^{-1} \sqrt{\frac{k_p - k_a}{k_a}}$$

Substituting values gives

$$R_{\text{sen}} = \frac{4 \times 50 \times 10^{-9} \text{ m}}{\pi \times (100 \times 10^{-9} \text{ m})^2} \times \frac{1}{\sqrt{0.0263 \text{ W/m} \cdot \text{K} \times (1.38 - 0.0263) \text{ W/m} \cdot \text{K}}} \\ \times \tan^{-1} \sqrt{\frac{(1.38 - 0.0263) \text{ W/m} \cdot \text{K}}{0.0263 \text{ W/m} \cdot \text{K}}} = 48.3 \times 10^6 \text{ K/W} <$$

(b) The thermal circuit is



Hence,

$$\frac{(T_{\text{surf}} - T_{\text{sen}})}{R_{\text{sen}}} = \frac{(T_{\text{sen}} - T_{\infty})}{R_T}$$

$$T_{\text{surf}} = (T_{\text{sen}} - T_{\infty}) \cdot \frac{R_{\text{sen}}}{R_T} + T_{\text{sen}} = (28.5 - 25)^{\circ}\text{C} \times \frac{48.3 \times 10^6 \text{ K/W}}{5 \times 10^6 \text{ K/W}} + 28.5^{\circ}\text{C}$$

$$T_{\text{surf}} = 62.3^{\circ}\text{C}$$

**COMMENT:** Heat transfer within the probe region will not be one-dimensional and modification of heat transfer due to nanoscale effects may be important. However, the probe may be calibrated by measuring the surface temperature of a large isothermal object.