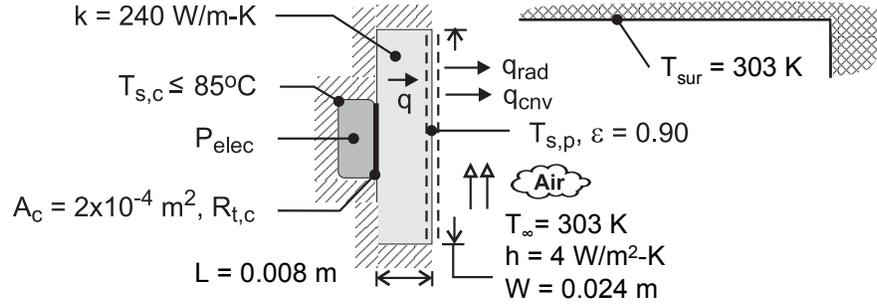


PROBLEM 3.33

KNOWN: Dimensions, thermal conductivity and emissivity of base plate. Temperature and convection coefficient of adjoining air. Temperature of surroundings. Maximum allowable temperature of transistor case. Case-plate interface conditions.

FIND: (a) Maximum allowable power dissipation for an air-filled interface, (b) Effect of convection coefficient on maximum allowable power dissipation.

SCHEMATIC:



ASSUMPTIONS: (1) Steady-state, (2) Negligible heat transfer from the enclosure, to the surroundings. (3) One-dimensional conduction in the base plate, (4) Radiation exchange at surface of base plate is with large surroundings, (5) Constant thermal conductivity.

PROPERTIES: Aluminum-aluminum interface, air-filled, 10^5 N/m^2 contact pressure (Table 3.1): $R_{t,c}'' = 2.75 \times 10^{-4} \text{ m}^2 \cdot \text{K} / \text{W}$.

ANALYSIS: (a) With all of the heat dissipation transferred through the base plate,

$$P_{\text{elec}} = q = \frac{T_{s,c} - T_\infty}{R_{\text{tot}}} \quad (1)$$

where $R_{\text{tot}} = R_{t,c} + R_{\text{cnd}} + \left[\left(\frac{1}{R_{\text{cnv}}} \right) + \left(\frac{1}{R_{\text{rad}}} \right) \right]^{-1}$

$$R_{\text{tot}} = \frac{R_{t,c}''}{A_c} + \frac{L}{kW^2} + \frac{1}{W^2} \left(\frac{1}{h + h_r} \right) \quad (2)$$

$$\text{and } h_r = \epsilon \sigma (T_{s,p} + T_{\text{sur}}) (T_{s,p}^2 + T_{\text{sur}}^2) \quad (3)$$

To obtain $T_{s,p}$, the following energy balance must be performed on the plate surface,

$$q = \frac{T_{s,c} - T_{s,p}}{R_{t,c} + R_{\text{cnd}}} = q_{\text{cnv}} + q_{\text{rad}} = hW^2 (T_{s,p} - T_\infty) + h_r W^2 (T_{s,p} - T_{\text{sur}}) \quad (4)$$

With $R_{t,c} = 2.75 \times 10^{-4} \text{ m}^2 \cdot \text{K} / \text{W} / 2 \times 10^{-4} \text{ m}^2 = 1.375 \text{ K} / \text{W}$, $R_{\text{cnd}} = 0.008 \text{ m} / (240 \text{ W} / \text{m} \cdot \text{K} \times 5.76 \times 10^{-4} \text{ m}^2) = 0.0579 \text{ K} / \text{W}$, and the prescribed values of h , W , $T_\infty = T_{\text{sur}}$ and ϵ , Eq. (4) yields a surface temperature of $T_{s,p} = 357.5 \text{ K} = 84.5^\circ \text{C}$ and a power dissipation of

Continued ...

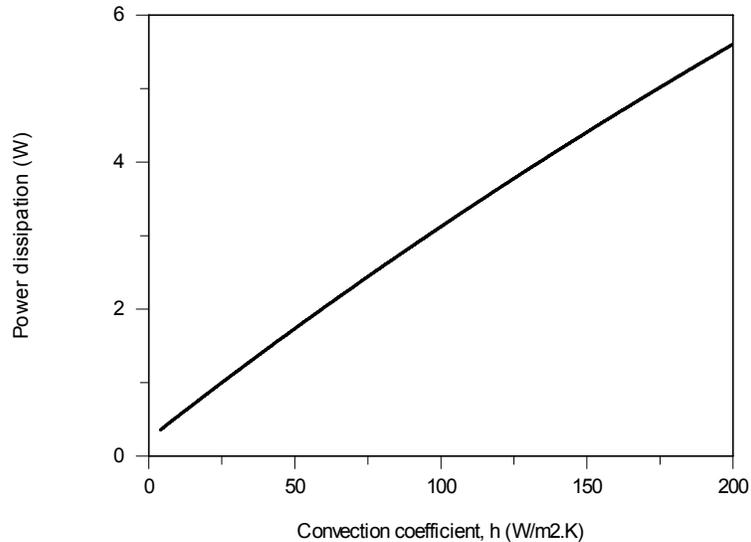
PROBLEM 3.33 (Cont.)

$$P_{\text{elec}} = q = 0.358 \text{ W}$$

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The convection and radiation resistances are $R_{\text{cnv}} = 434 \text{ K/W}$ and $R_{\text{rad}} = 235 \text{ K/W}$, where $h_f = 7.40 \text{ W/m}^2 \cdot \text{K}$.

(b) With the major contribution to the total resistance made by convection, significant benefit may be derived by increasing the value of h .



For $h = 200 \text{ W/m}^2 \cdot \text{K}$, $R_{\text{cnv}} = 8.68 \text{ K/W}$ and $T_{\text{s,p}} = 350 \text{ K}$, yielding $R_{\text{rad}} = 243 \text{ K/W}$. The effect of radiation is then negligible.

COMMENTS: (1) The plate conduction resistance is negligible, and even for $h = 200 \text{ W/m}^2 \cdot \text{K}$, the contact resistance is small relative to the convection resistance. However, $R_{\text{t,c}}$ could be rendered negligible by using indium foil, instead of an air gap, at the interface. From Table 3.1, $R_{\text{t,c}}'' = 0.07 \times 10^{-4} \text{ m}^2 \cdot \text{K/W}$, in which case $R_{\text{t,c}} = 0.035 \text{ m} \cdot \text{K/W}$.

(2) Because $A_c < W^2$, heat transfer by conduction in the plate is actually two-dimensional, rendering the conduction resistance even smaller.