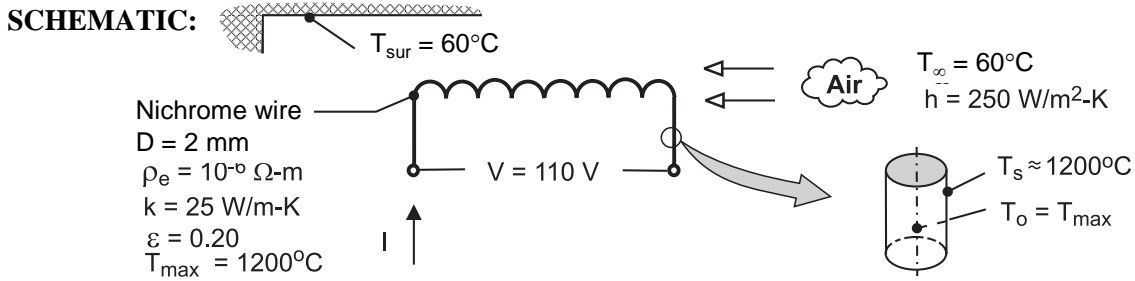


PROBLEM 3.86

KNOWN: Diameter, resistivity, thermal conductivity, emissivity, voltage, and maximum temperature of heater wire. Convection coefficient and air exit temperature. Temperature of surroundings.

FIND: Maximum operating current, heater length and power rating.



ASSUMPTIONS: (1) Steady-state, (2) Uniform wire temperature, (3) Constant properties, (4) Radiation exchange with large surroundings.

ANALYSIS: Assuming a uniform wire temperature, $T_{\max} = T(r=0) \equiv T_o \approx T_s$, the maximum volumetric heat generation may be obtained from Eq. (3.60), but with the total heat transfer coefficient, $h_t = h + h_r$, used in lieu of the convection coefficient h . With

$$h_r = \varepsilon \sigma (T_s + T_{\text{sur}}) (T_s^2 + T_{\text{sur}}^2) = 0.20 \times 5.67 \times 10^{-8} \text{ W/m}^2 \cdot \text{K}^4 (1473 + 333) \text{ K} (1473^2 + 333^2) \text{ K}^2 = 46.7 \text{ W/m}^2 \cdot \text{K}$$

$$h_t = (250 + 46.7) \text{ W/m}^2 \cdot \text{K} = 296.7 \text{ W/m}^2 \cdot \text{K}$$

$$\dot{q}_{\max} = \frac{2h_t}{r_o} (T_s - T_\infty) = \frac{2(296.7 \text{ W/m}^2 \cdot \text{K})}{0.001 \text{ m}} (1140^\circ\text{C}) = 6.76 \times 10^8 \text{ W/m}^3$$

Hence, with $\dot{q} = \frac{I^2 R_e}{V} = \frac{I^2 (\rho_e L / A_c)}{LA_c} = \frac{I^2 \rho_e}{A_c^2} = \frac{I^2 \rho_e}{(\pi D^2 / 4)^2}$

$$I_{\max} = \left(\frac{\dot{q}_{\max}}{\rho_e} \right)^{1/2} \frac{\pi D^2}{4} = \left(\frac{6.76 \times 10^8 \text{ W/m}^3}{10^{-6} \Omega \cdot \text{m}} \right)^{1/2} \frac{\pi (0.002 \text{ m})^2}{4} = 81.7 \text{ A} \quad <$$

Also, with $\Delta E = I R_e = I (\rho_e L / A_c)$,

$$L = \frac{\Delta E \cdot A_c}{I_{\max} \rho_e} = \frac{110 \text{ V} \left[\pi (0.002 \text{ m})^2 / 4 \right]}{81.7 \text{ A} (10^{-6} \Omega \cdot \text{m})} = 4.23 \text{ m} \quad <$$

and the power rating is

$$P_{\text{elec}} = \Delta E \cdot I_{\max} = 110 \text{ V} (81.7 \text{ A}) = 8990 \text{ W} = 8.99 \text{ kW} \quad <$$

COMMENTS: To assess the validity of assuming a uniform wire temperature, Eq. (3.58) may be used to compute the centerline temperature corresponding to \dot{q}_{\max} and a surface temperature of

$$1200^\circ\text{C}. \text{ It follows that } T_o = \frac{\dot{q} r_o^2}{4k} + T_s = \frac{6.76 \times 10^8 \text{ W/m}^3 (0.001 \text{ m})^2}{4(25 \text{ W/m} \cdot \text{K})} + 1200^\circ\text{C} = 1207^\circ\text{C}. \text{ With only a}$$

7°C temperature difference between the centerline and surface of the wire, the assumption is excellent.