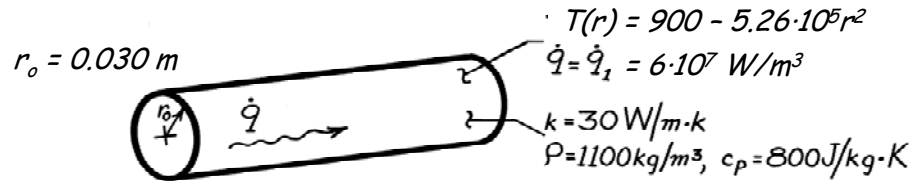


## PROBLEM 2.28

**KNOWN:** Steady-state temperature distribution in a cylindrical rod having uniform heat generation of  $\dot{q}_1 = 6 \times 10^7 \text{ W/m}^3$ .

**FIND:** (a) Steady-state centerline and surface heat transfer rates per unit length,  $q'_r$ . (b) Initial time rate of change of the centerline and surface temperatures in response to a change in the generation rate from  $\dot{q}_1$  to  $\dot{q}_2 = 10^8 \text{ W/m}^3$ .

**SCHEMATIC:**



**ASSUMPTIONS:** (1) One-dimensional conduction in the  $r$  direction, (2) Uniform generation, and (3) Steady-state for  $\dot{q}_1 = 6 \times 10^7 \text{ W/m}^3$ .

**ANALYSIS:** (a) From the rate equations for cylindrical coordinates,

$$q_r'' = -k \frac{\partial T}{\partial r} \quad q = -kA_r \frac{\partial T}{\partial r}.$$

Hence,

$$q_r = -k(2\pi rL) \frac{\partial T}{\partial r}$$

or

$$q_r' = -2\pi k r \frac{\partial T}{\partial r} \tag{1}$$

where  $\partial T / \partial r$  may be evaluated from the prescribed temperature distribution,  $T(r)$ .

At  $r = 0$ , the gradient is  $(\partial T / \partial r) = 0$ . Hence, from Equation (1) the heat rate is

$$q_r'(0) = 0. \quad <$$

At  $r = r_o$ , the temperature gradient is

$$\begin{aligned} \left. \frac{\partial T}{\partial r} \right|_{r=r_o} &= -2 \left[ 5.26 \times 10^5 \frac{\text{K}}{\text{m}^2} \right] (r_o) = -2 (5.26 \times 10^5) (0.030 \text{ m}) \\ \left. \frac{\partial T}{\partial r} \right|_{r=r_o} &= -31.6 \times 10^3 \text{ K/m}. \end{aligned}$$

Continued ...

### PROBLEM 2.28 (Cont.)

Hence, the heat rate at the outer surface ( $r = r_o$ ) per unit length is

$$q'_r(r_o) = -2\pi [30 \text{ W/m} \cdot \text{K}] (0.030 \text{ m}) \left[ -31.6 \times 10^3 \text{ K/m} \right]$$

$$q'_r(r_o) = 1.785 \times 10^5 \text{ W/m.}$$

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(b) Transient (time-dependent) conditions will exist when the generation is changed, and for the prescribed assumptions, the temperature is determined by the following form of the heat equation, Equation 2.26

$$\frac{1}{r} \frac{\partial}{\partial r} \left[ kr \frac{\partial T}{\partial r} \right] + \dot{q}_2 = \rho c_p \frac{\partial T}{\partial t}$$

Hence

$$\frac{\partial T}{\partial t} = \frac{1}{\rho c_p} \left[ \frac{1}{r} \frac{\partial}{\partial r} \left[ kr \frac{\partial T}{\partial r} \right] + \dot{q}_2 \right].$$

However, initially (at  $t = 0$ ), the temperature distribution is given by the prescribed form,  $T(r) = 800 - 5.26 \times 10^5 r^2$ , and

$$\begin{aligned} \frac{1}{r} \frac{\partial}{\partial r} \left[ kr \frac{\partial T}{\partial r} \right] &= \frac{k}{r} \frac{\partial}{\partial r} \left[ r \left( -10.52 \times 10^5 \cdot r \right) \right] \\ &= \frac{k}{r} \left( -21.04 \times 10^5 \cdot r \right) \\ &= 30 \text{ W/m} \cdot \text{K} \left[ -21.04 \times 10^5 \text{ K/m}^2 \right] \\ &= -6.31 \times 10^7 \text{ W/m}^3 \text{ (the original } \dot{q} = \dot{q}_1 \text{).} \end{aligned}$$

Hence, everywhere in the wall,

$$\frac{\partial T}{\partial t} = \frac{1}{1100 \text{ kg/m}^3 \times 800 \text{ J/kg} \cdot \text{K}} \left[ -6.31 \times 10^7 + 10^8 \right] \text{ W/m}^3$$

or

$$\frac{\partial T}{\partial t} = 41.91 \text{ K/s}$$

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**COMMENTS:** (1) The value of  $(\partial T / \partial t)$  will decrease with increasing time, until a new steady-state condition is reached and once again  $(\partial T / \partial t) = 0$ . (2) By applying the energy conservation requirement, Equation 1.12c, to a unit length of the rod for the steady-state condition,  $\dot{E}'_{\text{in}} - \dot{E}'_{\text{out}} + \dot{E}'_{\text{gen}} = 0$ .

$$\text{Hence } q'_r(0) - q'_r(r_o) = -\dot{q}_1 (\pi r_o^2).$$