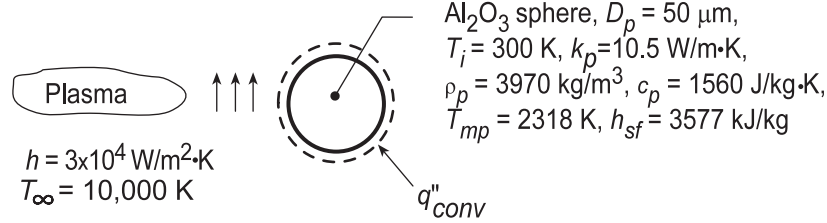


## PROBLEM 5.25

**KNOWN:** Diameter and thermophysical properties of alumina particles. Convection conditions associated with a two-step heating process.

**FIND:** (a) Time-in-flight ( $t_{i-f}$ ) required for complete melting, (b) Validity of assuming negligible radiation.

**SCHEMATIC:**



**ASSUMPTIONS:** (1) Particle behaves as a lumped capacitance, (2) Negligible radiation, (3) Constant properties.

**ANALYSIS:** (a) The two-step process involves (i) the time  $t_1$  to heat the particle to its melting point and (ii) the time  $t_2$  required to achieve complete melting. Hence,  $t_{i-f} = t_1 + t_2$ , where from Eq. (5.5),

$$t_1 = \frac{\rho_p V c_p}{h A_s} \ln \frac{\theta_i}{\theta} = \frac{\rho_p D_p c_p}{6h} \ln \frac{T_i - T_\infty}{T_{mp} - T_\infty}$$

$$t_1 = \frac{3970 \text{ kg/m}^3 (50 \times 10^{-6} \text{ m}) 1560 \text{ J/kg} \cdot \text{K}}{6 (30,000 \text{ W/m}^2 \cdot \text{K})} \ln \frac{(300 - 10,000)}{(2318 - 10,000)} = 4 \times 10^{-4} \text{ s}$$

Performing an energy balance for the second step, we obtain

$$\int_{t_1}^{t_1+t_2} q_{conv} dt = \Delta E_{st}$$

where  $q_{conv} = h A_s (T_\infty - T_{mp})$  and  $\Delta E_{st} = \rho_p V h_{sf}$ . Hence,

$$t_2 = \frac{\rho_p D_p}{6h} \frac{h_{sf}}{(T_\infty - T_{mp})} = \frac{3970 \text{ kg/m}^3 (50 \times 10^{-6} \text{ m})}{6 (30,000 \text{ W/m}^2 \cdot \text{K})} \times \frac{3.577 \times 10^6 \text{ J/kg}}{(10,000 - 2318) \text{ K}} = 5 \times 10^{-4} \text{ s}$$

Hence  $t_{i-f} = 9 \times 10^{-4} \text{ s} \approx 1 \text{ ms}$

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(b) Contrasting the smallest value of the convection heat flux,  $q''_{conv,min} = h (T_\infty - T_{mp}) = 2.3 \times 10^8 \text{ W/m}^2$  to the largest radiation flux,  $q''_{rad,max} = \varepsilon \sigma (T_{mp}^4 - T_{sur}^4) = 6.7 \times 10^5 \text{ W/m}^2$ , with  $\varepsilon = 0.41$  from Table A.8 for aluminum oxide at 1500 K, and  $T_{sur} = 300 \text{ K}$  we conclude that radiation is, in fact, negligible.

**COMMENTS:** (1) Since  $Bi = (hr_p/3)/k \approx 0.02$ , the lumped capacitance assumption is good. (2) In an actual application, the droplet should impact the substrate in a superheated condition ( $T > T_{mp}$ ), which would require a slightly larger  $t_{i-f}$ .