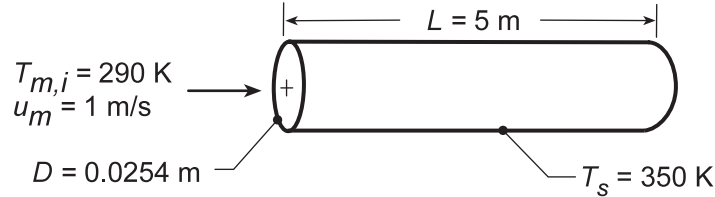


PROBLEM 8.49

KNOWN: Diameter, length and surface temperature of condenser tubes. Water velocity and inlet temperature.

FIND: (a) Water outlet temperature evaluating properties at $T_m = 300$ K, (b) Repeat calculations using properties evaluated at the appropriate temperature, $\bar{T}_m = (T_{m,i} + T_{m,o})/2$, and (c) Coolant mean velocities for the range $4 \leq L \leq 7$ m which provide the same $T_{m,o}$ as found in part (b).

SCHEMATIC:



ASSUMPTIONS: (1) Negligible tube wall conduction resistance, (2) Incompressible liquid with negligible viscous dissipation.

PROPERTIES: Table A.6, Water ($\bar{T}_m = 300$ K): $\rho = 997$ kg/m³, $c_p = 4179$ J/kg·K, $\mu = 855 \times 10^{-6}$ kg/s·m, $k = 0.613$ W/m·K, $Pr = 5.83$.

ANALYSIS: (a) From Equation 8.41b

$$T_{m,o} = T_s - (T_s - T_{m,i}) \exp \left[- \left(\pi D L / \dot{m} c_p \right) \bar{h} \right].$$

and evaluating properties at $\bar{T}_m = 300$ K, find

$$Re_D = \frac{\rho u_m D}{\mu} = \frac{997 \text{ kg/m}^3 (1 \text{ m/s}) (0.0254 \text{ m})}{855 \times 10^{-6} \text{ kg/s} \cdot \text{m}} = 29,618$$

The flow is turbulent, and since $L/D = 197$, it is reasonable to assume fully developed flow throughout the tube. Hence, $\bar{h} \approx h_{fd}$. From the Dittus-Boelter equation,

$$Nu_D = 0.023 Re_D^{4/5} Pr^{0.4} = 0.023 (29,618)^{4/5} (5.83)^{0.4} = 176$$

$$\bar{h} = Nu_D (k/D) = 176 (0.613 \text{ W/m} \cdot \text{K} / 0.0254 \text{ m}) = 4248 \text{ W/m}^2 \cdot \text{K}.$$

With

$$\dot{m} = \rho u_m \left(\pi D^2 / 4 \right) = (\pi/4) 997 \text{ kg/m}^3 (1 \text{ m/s}) (0.0254 \text{ m})^2 = 0.505 \text{ kg/s}.$$

Equation 8.41b yields

$$T_{m,o} = 350 \text{ K} - (60 \text{ K}) \exp \left[- \frac{\pi (0.0254 \text{ m}) 5 \text{ m} (4248 \text{ W/m}^2 \cdot \text{K})}{0.505 \text{ kg/s} (4179 \text{ J/kg} \cdot \text{K})} \right] = 323 \text{ K} = 50^\circ \text{C} \quad <$$

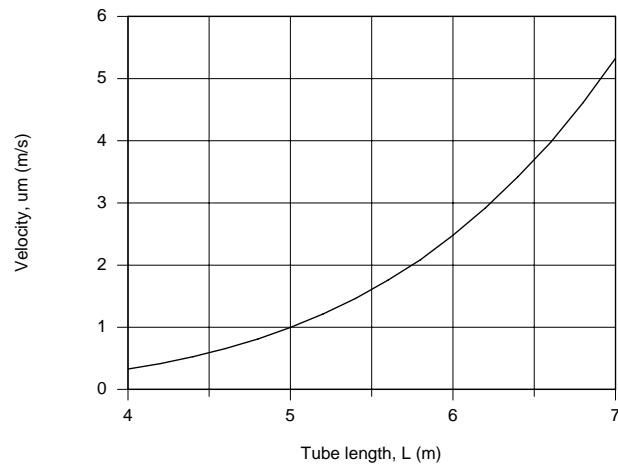
(b) Using the *IHT Correlations Tool, Internal Flow*, for fully developed *Turbulent Flow*, along with the energy balance and rate equations above, the calculation of part (a) is repeated with $\bar{T}_m = (T_{m,i} + T_{m,o})/2$ giving these results:

$$\bar{T}_m = 307.3 \text{ K} \quad T_{m,o} = 51.7^\circ \text{C} = 324.7 \text{ K} \quad <$$

(c) Using the IHT model developed for the part (b) analysis, the coolant mean velocity, u_m , as a function of tube length L with $T_{m,o} = 51.7^\circ \text{C}$ is calculated and the results plotted below.

Continued...

PROBLEM 8.49 (Cont.)



COMMENTS: (1) Using $\bar{T}_m = 300$ K vs. $\bar{T}_m = (T_{m,i} + T_{m,o})/2 = 307$ K for this application resulted in a difference of $T_{m,o} = 50^\circ\text{C}$ vs. $T_{m,o} = 51.7^\circ\text{C}$. While the difference is only 1.7°C , it is good practice to use the proper value for \bar{T}_m .

(2) Note that u_m must be increased markedly with increasing length in order that $T_{m,o}$ remain fixed.