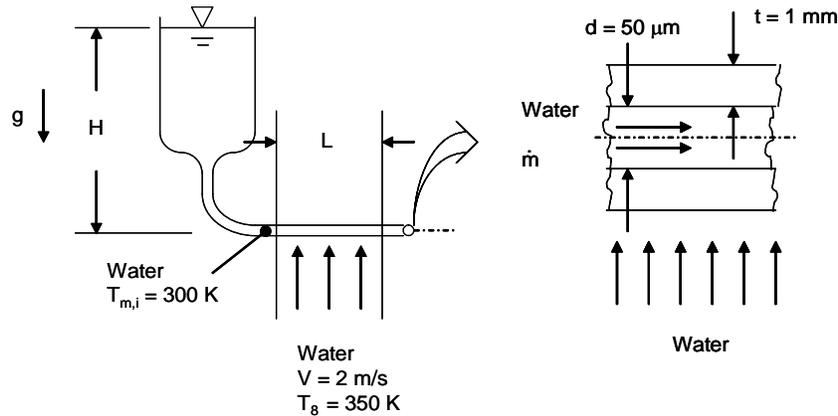


## PROBLEM 8.115

**KNOWN:** Inner diameter of microscale tube, wall thickness of tube, temperature of water inside the tube, and temperature of water in cross flow over the tube.

**FIND:** (a) Required tube length at  $Re_D = 2000$ , (b) Water outlet temperature, (c) Pressure drop associated with the flow of water inside the tube, (d) Height of water column needed to supply the required inlet pressure and time needed to collect 0.1 liter of water. Discuss measurement of outlet water temperature.

**SCHEMATIC:**



**ASSUMPTIONS:** (1) Constant properties and steady-state conditions, (2) Incompressible liquid and negligible viscous dissipation, (3) Negligible microscale or nanoscale effects.

**PROPERTIES:** Table A.6, water: ( $\bar{T}_m = 305$  K):  $k = 0.620$  W/m·K,  $c_p = 4178$  J/kg·K,  $\mu = 769 \times 10^{-6}$  N·s/m<sup>2</sup>,  $Pr = 5.2$ ,  $\rho = 995$  kg/m<sup>3</sup>; ( $\bar{T} = 330$  K):  $k = 0.650$  W/m·K,  $c_p = 4194$  J/kg·K,  $\mu = 489 \times 10^{-6}$  N·s/m<sup>2</sup>,  $Pr = 3.15$ ,  $\rho = 984$  kg/m<sup>3</sup>. Table A.3 glass:  $k = 1.4$  W/m·K.

**ANALYSIS:** (a) At  $Re_D = 2000$ , Equation 8.3 yields  $x_{fd,h} = 0.05Re_DPrD = 0.05 \times 2000 \times 5.2 \times 50 \times 10^{-6}$  m =  $26 \times 10^{-3}$  m. Therefore,  $L = 2x_{fd,h} = 2 \times 26 \times 10^{-3}$  m =  $52 \times 10^{-3}$  m = 52 mm. <

(b) Equation 8.45a is

$$\frac{T_{\infty} - T_{m,o}}{T_{\infty} - T_{m,i}} = \exp\left(-\frac{\bar{U}A_s}{\dot{m}c_p}\right) \quad (1)$$

where we will use  $\bar{U} = \bar{U}_i$ ,  $A_s = A_{s,i}$ . Note that  $Re_D = 4\dot{m}/(\pi D\mu)$  so that  $\dot{m} = Re_D \pi D\mu / 4 = 2000 \times \pi \times 50 \times 10^{-6}$  m  $\times 769 \times 10^{-6}$  N·s/m<sup>2</sup>/4 =  $60.4 \times 10^{-6}$  kg/s. Therefore,  $u_m = \dot{m}/(\rho A_c) = 60.4 \times 10^{-6}$  kg/s  $\times 4 / (995$  kg/m<sup>3</sup>  $\times \pi \times (50 \times 10^{-6}$  m)<sup>2</sup>) = 31 m/s. From Equation 3.36,

Continued...

**PROBLEM 8.115 (Cont.)**

$$\bar{U}_i = \frac{1}{\frac{1}{h_i} + \frac{d/2}{k_g} \ln \left[ \frac{(d/2+t)}{d/2} \right] + \frac{d/2}{(d/2+t)} \frac{1}{h_o}} \quad (2)$$

$A_{s,i} = \pi dL = \pi \times 50 \times 10^{-6} \text{ m} \times 52 \times 10^{-3} \text{ m} = 8.17 \times 10^{-6} \text{ m}^2$ . From Equation 8.56,

$$\bar{Nu}_D = 3.66 + \frac{0.0668(50 \times 10^{-6} / 53 \times 10^{-3}) \times 2000 \times 5.3}{1 + 0.04 \left[ (50 \times 10^{-6} / 53 \times 10^{-3}) \times 2000 \times 5.3 \right]^{2/3}} = 4.371$$

and  $\bar{h}_D = h_i = \bar{Nu}_D \frac{k}{D} = 4.371 \times 0.620 \text{ W/m} \cdot \text{K} / 50 \times 10^{-6} \text{ m} = 54.2 \times 10^3 \text{ W/m}^2 \cdot \text{K}$ .

For the cross flow of water over the tube,  $Re_D = VD\rho/\mu = 2 \text{ m/s} \times (50 \times 10^{-6} \text{ m} + 2 \times 1 \times 10^{-3} \text{ m})(984 \text{ kg/m}^3)/489 \times 10^{-6} \text{ N}\cdot\text{s/m}^2 = 8253$ . From Equation 7.46,

$$\bar{Nu}_D = 0.3 + \frac{0.62(8253)^{1/2}(3.15)^{1/3}}{\left[ 1 + (0.4/3.15)^{2/3} \right]^{1/4}} \left[ 1 + \left( \frac{8253}{282,000} \right)^{5/8} \right]^{4/5} = 85.14$$

and

$\bar{h}_D = h_o = \bar{Nu}_D k / (d + 2t) = 85.14 \times 0.65 \text{ W/m} \cdot \text{K} / (50 \times 10^{-6} \text{ m} + 2 \times 1 \times 10^{-3} \text{ m}) = 27.0 \times 10^3 \text{ W/m}^2 \cdot \text{K}$

Therefore,

$$\bar{U}_i = \frac{1}{\left[ \frac{1}{54.2 \times 10^3 \text{ W/m} \cdot \text{K}} + \frac{50 \times 10^{-6} \text{ m}/2}{1.4 \text{ W/m} \cdot \text{K}} \ln \left[ \frac{(50 \times 10^{-6} \text{ m}/2 + 1 \times 10^{-3} \text{ m})}{50 \times 10^{-6} \text{ m}/2} \right] \right] + \frac{50 \times 10^{-6} \text{ m}/2}{(50 \times 10^{-6} \text{ m}/2 + 1 \times 10^{-3} \text{ m})} \times \frac{1}{27.0 \times 10^3 \text{ W/m}^2 \cdot \text{K}}} = 11.7 \times 10^3 \text{ W/m}^2 \cdot \text{K}$$

Equation (1) becomes

$$\frac{350\text{K} - T_{m,o}}{350\text{K} - 300\text{K}} = \exp \left( - \frac{11.7 \times 10^3 \text{ W/m}^2 \cdot \text{K} \times 8.17 \times 10^{-6} \text{ m}^2}{60.4 \times 10^{-6} \text{ kg/s} \cdot 4194 \text{ J/kg} \cdot \text{K}} \right)$$

or,  $T_{m,o} = 316 \text{ K}$

<  
Continued...

### PROBLEM 8.115 (Cont.)

(c) For laminar flow, Equation 8.19 yields  $f = 64/\text{Re}_D = 64/2000 = 32 \times 10^{-3}$ . Equation 8.22a yields

$$\Delta p = f \frac{\rho u_m^2}{2D} L = \frac{32 \times 10^{-3} \times 995 \text{ kg/m}^3 \times (31 \text{ m/s})^2 \times 52 \times 10^{-3} \text{ m}}{2(50 \times 10^{-6} \text{ m})} = 15.9 \times 10^6 \text{ Pa} \quad <$$

(d) The pressure generated by the water column must offset the pressure drop in the tube. Therefore,

$$\rho g H = \Delta p \quad \text{or} \quad H = \Delta p / \rho g = 15.9 \times 10^6 \text{ N/m}^2 / (995 \text{ kg/m}^3 \times 9.8 \text{ m/s}^2) = 1630 \text{ m} = 1.63 \text{ km} \quad <$$

The time required for a particular volume of water to flow through the system is

$$t = \frac{V\rho}{m} = \frac{0.1 \times \frac{1 \text{ m}^3}{1000 \text{ ml}} \times 995 \text{ kg/m}^3}{60.4 \times 10^{-6} \text{ kg/s}} = 1650 \text{ s} \quad <$$

**COMMENTS:** (1) Microscale experimentation is often very difficult to perform. In addition to the difficulty in measuring the water outlet temperature, establishing a constant flow rate with such a large inlet pressure would be very difficult. (2) Turbulent conditions in microscale systems are rare in nature, and are difficult to achieve experimentally. (3) The glass tube wall is relatively thick. Therefore, conduction in the axial direction is likely to be significant. (4) The average mean water temperature inside the tube is  $\bar{T}_m = (T_{m,i} + T_{m,o})/2 = (300 \text{ K} + 316 \text{ K})/2 = 308 \text{ K}$ . The assumed mean temperature of 305 K is good.