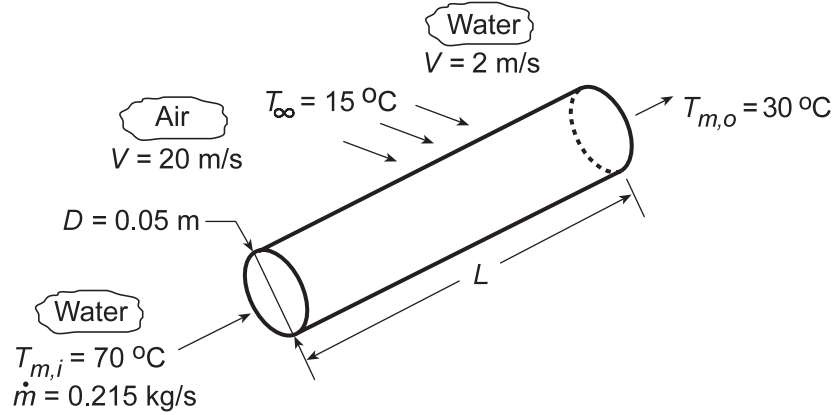


PROBLEM 8.62

KNOWN: Diameter of tube through which water of prescribed flow rate and inlet and outlet temperatures flows. Temperature of fluid in cross flow over the tube.

FIND: (a) Required tube length for air in cross flow at prescribed velocity, (b) Required tube length for water in cross flow at a prescribed velocity.

SCHEMATIC:



ASSUMPTIONS: (1) Steady-state, (2) Constant properties, (3) Negligible tube wall conduction resistance, (4) Water is incompressible liquid with negligible viscous dissipation.

PROPERTIES: Table A.6, water ($\bar{T}_m = 50^\circ\text{C} = 323\text{ K}$): $c_p = 4181\text{ J/kg}\cdot\text{K}$, $\mu = 548 \times 10^{-6}\text{ N}\cdot\text{s/m}^2$, $k = 0.643\text{ W/m}\cdot\text{K}$, $\text{Pr} = 3.56$. Table A.4, air (assume $T_f = 300\text{ K}$): $\nu = 15.89 \times 10^{-6}\text{ m}^2/\text{s}$, $k = 0.0263\text{ W/m}\cdot\text{K}$, $\text{Pr} = 0.707$. Table A.6, water (assume $T_f = 300\text{ K}$): $\nu = 0.858 \times 10^{-6}\text{ m}^2/\text{s}$, $k = 0.613\text{ W/m}\cdot\text{K}$, $\text{Pr} = 5.83$.

ANALYSIS: The required heat rate may be determined from the overall energy balance,

$$q = \dot{m}c_p(T_{m,i} - T_{m,o}) = 0.215\text{ kg/s}(4181\text{ J/kg}\cdot\text{K})40^\circ\text{C} = 35,960\text{ W}$$

and the required tube length may be determined from the rate equation, Eq. 8.46a,

$$L = \frac{q}{U\pi D\Delta T_{\ell m}}$$

where

$$\Delta T_{\ell m} = \frac{(T_{m,i} - T_\infty) - (T_{m,o} - T_\infty)}{\ln\left(\frac{T_{m,i} - T_\infty}{T_{m,o} - T_\infty}\right)} = 30.8^\circ\text{C} \quad \text{and} \quad 1/U = 1/h_i + 1/h_o.$$

With

$$\text{Re}_{D_i} = 4\dot{m}/\pi D\mu = 0.860\text{ kg/s}/\pi(0.05\text{ m})548 \times 10^{-6}\text{ N}\cdot\text{s/m}^2 = 9991$$

the flow is turbulent and, assuming fully developed flow throughout the tube, the inside convection coefficient is determined from Eq. 8.62

$$\text{Nu}_{D_i} = \frac{(f/8)(\text{Re}_{D_i} - 1000)\text{Pr}}{1 + 12.7(f/8)^{1/2}(\text{Pr}^{2/3} - 1)} = \frac{(0.0315/8)(9991 - 1000)3.56}{1 + 12.7(0.0315/8)^{1/2}(3.56^{2/3} - 1)} = 61.1$$

where $f = (0.79 \ln \text{Re}_{D_i} + 1.64)^{-2} = 0.0315$

$$h_i = \text{Nu}_{D_i} k/D = 61.1(0.643\text{ W/m}\cdot\text{K})/0.05\text{ m} = 786\text{ W/m}^2\cdot\text{K}$$

Continued...

PROBLEM 8.62 (Cont.)

(a) For air in cross flow at 20 m/s, $\text{Re}_{D_o} = VD/\nu = 20 \text{ m/s}(0.05 \text{ m})/15.89 \times 10^{-6} \text{ m}^2/\text{s} = 62,933$. From the Churchill/Bernstein correlation, it follows that

$$\text{Nu}_{D_o} = 0.3 + \frac{0.62 \text{Re}_{D_o}^{1/2} \text{Pr}^{1/3}}{\left[1 + (0.4/\text{Pr})^{2/3}\right]^{1/4}} \left[1 + \left(\frac{\text{Re}_{D_o}}{282,000}\right)^{5/8}\right]^{4/5} = 158.7$$

$$h_o = \text{Nu}_{D_o} k/D = 158.7 (0.0263 \text{ W/m} \cdot \text{K}) / 0.05 \text{ m} = 83.5 \text{ W/m}^2 \cdot \text{K}$$

Hence, $U = (1/h_i + 1/h_o)^{-1} = 75.5 \text{ W/m}^2 \cdot \text{K}$ and

$$L = \frac{35,960 \text{ W}}{(75.5 \text{ W/m}^2 \cdot \text{K}) \pi (0.05 \text{ m}) 30.8^\circ \text{C}} = 98.5 \text{ m} \quad <$$

(b) For water in cross flow at 2 m/s, $\text{Re}_{D_o} = 2 \text{ m/s}(0.05 \text{ m})/0.858 \times 10^{-6} \text{ m}^2/\text{s} = 116,550$, and the correlation yields $\text{Nu}_{D_o} = 527.3$. Hence,

$$h_o = \text{Nu}_{D_o} k/D = 527.3 (0.613 \text{ W/m} \cdot \text{K}) / 0.05 \text{ m} = 6,465 \text{ W/m}^2 \cdot \text{K}$$

$$U = (1/h_i + 1/h_o)^{-1} = 701 \text{ W/m}^2 \cdot \text{K}$$

Hence,

$$L = \frac{35,960 \text{ W}}{(701 \text{ W/m}^2 \cdot \text{K}) \pi (0.05 \text{ m}) 30.8^\circ \text{C}} = 10.6 \text{ m} \quad <$$

COMMENTS: The foregoing results clearly indicate the superiority of water (relative to air) as a heat transfer fluid. Note the dominant contribution made by the smaller convection coefficient to the value of U in each of the two cases.