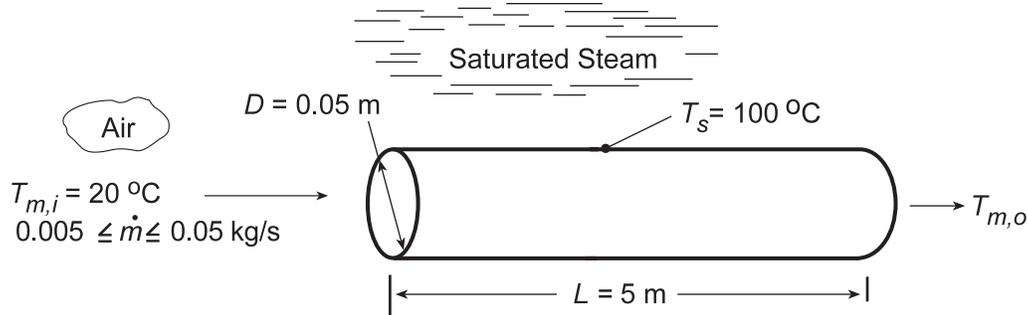


### PROBLEM 8.53

**KNOWN:** Diameter, length and surface temperature of tubes used to heat ambient air. Flow rate and inlet temperature of air.

**FIND:** (a) Air outlet temperature and heat rate per tube, (b) Effect of flow rate on outlet temperature. Design and operating conditions suitable for providing 1 kg/s of air at 75°C.

**SCHEMATIC:**



**ASSUMPTIONS:** (1) Steady-state, (2) Ideal gas with negligible viscous dissipation and pressure variation, (3) Negligible tube wall thermal resistance.

**PROPERTIES:** Table A.4, air (assume  $\bar{T}_m = 330$  K):  $c_p = 1008$  J/kg·K,  $\mu = 198.8 \times 10^{-7}$  N·s/m<sup>2</sup>,  $k = 0.0285$  W/m·K,  $Pr = 0.703$ .

**ANALYSIS:** (a) For  $\dot{m} = 0.01$  kg/s,  $Re_D = 4\dot{m}/\pi D\mu = 0.04$  kg/s/ $\pi(0.05$  m) $198.8 \times 10^{-7}$  N·s/m<sup>2</sup> = 12,810. Hence, the flow is turbulent. If fully developed flow is assumed throughout the tube, the Dittus-Boelter correlation may be used to obtain the average Nusselt number.

$$\bar{Nu}_D \approx Nu_D = 0.023 Re_D^{4/5} Pr^{0.4} = 0.023(12,810)^{0.8} (0.703)^{0.4} = 38.6$$

$$\text{Hence, } \bar{h} = \bar{Nu}_D (k/D) = 38.6(0.0285 \text{ W/m} \cdot \text{K}/0.05 \text{ m}) = 22.0 \text{ W/m}^2 \cdot \text{K}$$

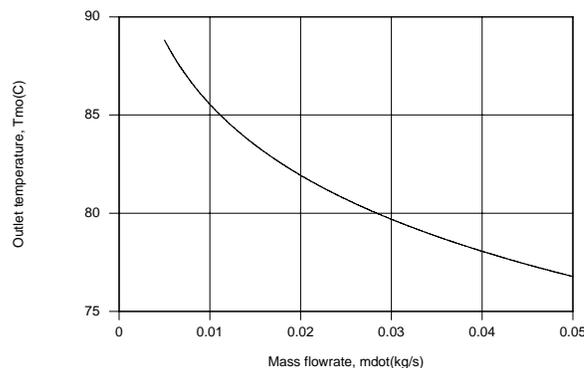
From Eq. 8.41b,

$$\frac{T_s - T_{m,o}}{T_s - T_{m,i}} = \exp\left(-\frac{\pi DL\bar{h}}{\dot{m}c_p}\right) = \exp\left(-\frac{\pi \times 0.05 \text{ m} \times 5 \text{ m} \times 22 \text{ W/m}^2 \cdot \text{K}}{0.01 \text{ kg/s} \times 1008 \text{ J/kg} \cdot \text{K}}\right) = 0.180$$

$$T_{m,o} = T_s - 0.180(T_s - T_{m,i}) = 100^\circ\text{C} - 0.180(80^\circ\text{C}) = 85.6^\circ\text{C} \quad <$$

$$\text{Hence, } q = \dot{m}c_p(T_{m,o} - T_{m,i}) = 0.01 \text{ kg/s}(1008 \text{ J/kg} \cdot \text{K})65.6 \text{ K} = 661 \text{ W} \quad <$$

(b) The effect of flow rate on the outlet temperature was determined by using the IHT *Correlations and Properties* Toolpads.



Continued...

### PROBLEM 8.53 (Cont.)

Although  $\bar{h}$  and hence the heat rate increase with increasing  $\dot{m}$ , the increase in  $q$  is not linearly proportional to the increase in  $\dot{m}$  and  $T_{m,o}$  decreases with increasing  $\dot{m}$ .

A flow rate of  $\dot{m} = 0.05 \text{ kg/s}$  is not large enough to provide the desired outlet temperature of  $75^\circ\text{C}$ , and to achieve this value, a flow rate of  $0.0678 \text{ kg/s}$  would be needed. At such a flow rate,  $N = 1 \text{ kg/s} / 0.0678 \text{ kg/s} = 14.75 \approx 15$  tubes would be needed to satisfy the process air requirement. Alternatively, a lower flow rate could be supplied to a larger number of tubes and the discharge mixed with ambient air to satisfy the desired conditions. Requirements of this option are that

$$N\dot{m} + \dot{m}_{\text{amb}} = 1 \text{ kg/s}$$

$$(N\dot{m} + \dot{m}_{\text{amb}})c_p(T_{m,o} - T_{m,i}) = 1 \text{ kg/s} \times 1008 \text{ J/kg} \cdot \text{K} (75 - 20) \text{ K} = 55,400 \text{ W}$$

where  $\dot{m}$  is the flow rate per tube. Using a larger number of tubes with a smaller flow rate per tube would reduce flow pressure losses and hence provide for reduced operating costs.

**COMMENTS:** With  $L/D = 5 \text{ m} / 0.05 \text{ m} = 100$ , the assumption of fully developed conditions throughout the tube is reasonable.