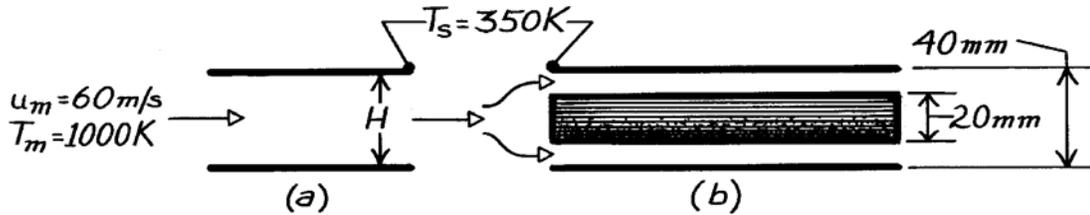


PROBLEM 8.84

KNOWN: Temperature and velocity of gas flow between parallel plates of prescribed surface temperature and separation. Thickness and location of plate insert.

FIND: Heat flux to the plates (a) without and (b) with the insert.

SCHEMATIC:



ASSUMPTIONS: (1) Steady-state conditions, (2) Negligible radiation, (3) Gas has properties of atmospheric air, (4) Plates are of infinite width W , (5) Fully developed flow.

PROPERTIES: Table A-4, Air (1 atm, $T_m = 1000$ K): $\rho = 0.348$ kg/m³, $\mu = 424.4 \times 10^{-7}$ kg/s·m, $k = 0.0667$ W/m·K, $Pr = 0.726$.

ANALYSIS: (a) Based upon the hydraulic diameter D_h , the Reynolds number is

$$D_h = 4 A_c / P = 4(H \cdot W) / 2(H + W) = 2H = 80 \text{ mm}$$

$$Re_{D_h} = \frac{\rho u_m D_h}{\mu} = \frac{0.348 \text{ kg/m}^3 (60 \text{ m/s}) 0.08 \text{ m}}{424.4 \times 10^{-7} \text{ kg/s} \cdot \text{m}} = 39,360.$$

Since the flow is fully developed and turbulent, use the Dittus-Boelter correlation,

$$Nu_D = 0.023 Re_D^{4/5} Pr^{0.3} = 0.023 (39,360)^{4/5} (0.726)^{0.3} = 99.1$$

$$h = \frac{k}{D_h} Nu_D = \frac{0.0667 \text{ W/m} \cdot \text{K}}{0.08 \text{ m}} 99.1 = 82.6 \text{ W/m}^2 \cdot \text{K}$$

$$q'' = h(T_m - T_s) = 82.6 \text{ W/m}^2 \cdot \text{K} (1000 - 350) \text{ K} = 53,700 \text{ W/m}^2. \quad <$$

(b) From continuity,

$$\dot{m} = (\rho u_m A)_a = (\rho u_m A)_b \quad u_m)_b = u_m)_a (\rho A)_a / (\rho A)_b = 60 \text{ m/s} (40/20) = 120 \text{ m/s}.$$

For each of the resulting channels, $D_h = 0.02$ m and

$$Re_{D_h} = \frac{\rho u_m D_h}{\mu} = \frac{0.348 \text{ kg/m}^3 (120 \text{ m/s}) 0.02 \text{ m}}{424.4 \times 10^{-7} \text{ kg/s} \cdot \text{m}} = 19,680.$$

Since the flow is still turbulent,

$$Nu_D = 0.023 (19,680)^{4/5} (0.726)^{0.3} = 56.9 \quad h = \frac{56.9 (0.0667 \text{ W/m} \cdot \text{K})}{0.02 \text{ m}} = 189.8 \text{ W/m}^2 \cdot \text{K}$$

$$q'' = 189.8 \text{ W/m}^2 \cdot \text{K} (1000 - 350) \text{ K} = 123,400 \text{ W/m}^2. \quad <$$

COMMENTS: From the Dittus-Boelter equation,

$$h_b / h_a = (u_{m,b} / u_{m,a})^{0.8} (D_{h,a} / D_{h,b})^{0.2} = (2)^{0.8} (4)^{0.2} = 1.74 \times 1.32 = 2.30.$$

Hence, heat transfer enhancement due to the insert is primarily a result of the increase in u_m and secondarily a result of the decrease in D_h .