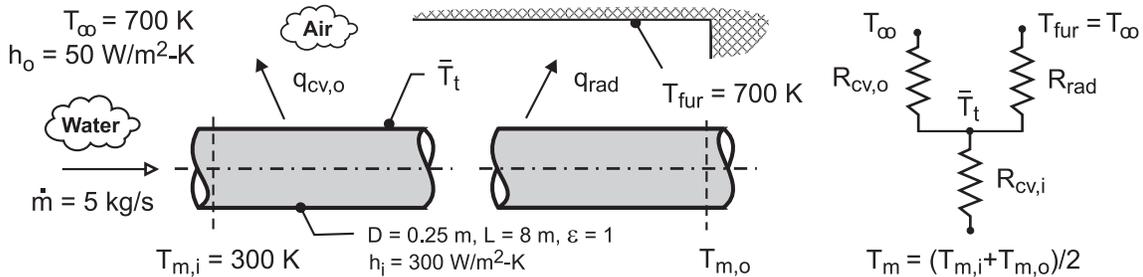


PROBLEM 8.20

KNOWN: Water at prescribed temperature and flow rate enters a 0.25 m diameter, black thin-walled tube of 8-m length, which passes through a large furnace whose walls and air are at a temperature of $T_{\text{fur}} = T_{\infty} = 700 \text{ K}$. The convection coefficients for the internal water flow and external furnace air are $300 \text{ W/m}^2\cdot\text{K}$ and $50 \text{ W/m}^2\cdot\text{K}$, respectively.

FIND: (a) An expression for the linearized radiation coefficient for the radiation exchange process between the outer surface of the pipe and the furnace walls; represent the tube by an average temperature and explain how to calculate this value, and (b) determine the outlet temperature of the water, T_{O} .

SCHEMATIC:



ASSUMPTIONS: (1) Steady-state conditions; (2) Tube is small object with large, isothermal surroundings; (3) Furnace air and walls are at the same temperature; (4) Tube is thin-walled with black surface; and (5) Incompressible liquid with negligible viscous dissipation.

PROPERTIES: Table A-6, Water ($T_m = (T_{m,i} + T_{m,o})/2 = 304 \text{ K}$): $c_p = 4178 \text{ J/kg}\cdot\text{K}$.

ANALYSIS: (a) The linearized radiation coefficient follows from Eq. 1.9 with $\epsilon = 1$,

$$\bar{h}_{\text{rad}} = \sigma (\bar{T}_t + T_{\text{fur}}) (\bar{T}_t^2 + T_{\text{fur}}^2)$$

where \bar{T}_t represents the average tube wall surface temperature, which can be evaluated from an energy balance on the tube as represented by the thermal circuit above.

$$T_m = (T_{m,i} + T_{m,o}) / 2$$

$$R_{\text{tot}} = R_{\text{cv},i} + \frac{1}{1/R_{\text{cv},o} + 1/R_{\text{rad}}}$$

$$\frac{T_m - \bar{T}_t}{R_{\text{cv},i}} = (\bar{T}_t - T_{\text{fur}}) (1/R_{\text{cv},o} + 1/R_{\text{rad}})$$

The thermal resistances, with $A_s = PL = \pi DL$, are

$$R_{\text{cv},i} = 1/h_i A_s \quad R_{\text{cv},o} = 1/h_o A_s \quad R_{\text{rad}} = 1/\bar{h}_{\text{rad}} A_s$$

(b) The outlet temperature can be calculated using the energy balance relation, Eq. 8.45b, with $T_{\text{fur}} = T_{\infty}$,

$$\frac{T_{\infty} - T_{m,o}}{T_{\infty} - T_{m,i}} = \exp\left(-\frac{1}{\dot{m} c_p R_{\text{tot}}}\right)$$

where c_p is evaluated at T_m . Using *IHT*, the following results were obtained.

$$R_{\text{cv},i} = 5.31 \times 10^{-4} \text{ K/W} \quad R_{\text{cv},o} = 3.18 \times 10^{-3} \text{ K/W} \quad R_{\text{rad}} = 3.96 \times 10^{-3} \text{ K/W}$$

$$T_m = 304 \text{ K} \quad \bar{T}_t = 396 \text{ K} \quad T_{m,o} = 308 \text{ K} \quad <$$

COMMENTS: Since $T_{\infty} = T_{\text{fur}}$, it was possible to use Eq. 8.45b with R_{tot} . How would you write the energy balance relation if $T_{\infty} \neq T_{\text{fur}}$?