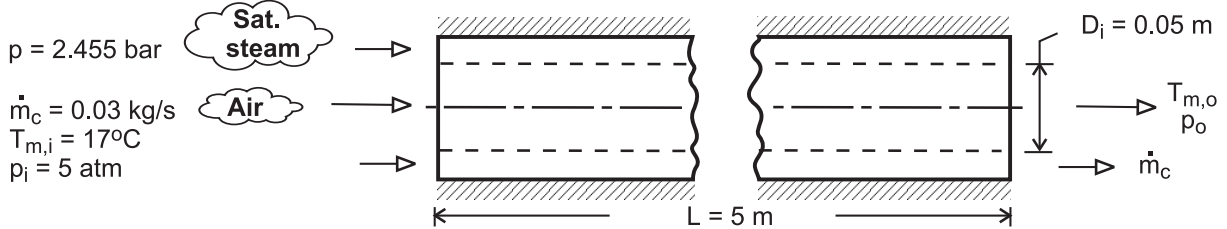


PROBLEM 8.38

KNOWN: Inlet temperature, pressure and flow rate of air. Tube diameter and length. Pressure of saturated steam.

FIND: Outlet temperature and pressure of air. Mass rate of steam condensation.

SCHEMATIC:



ASSUMPTIONS: (1) Steady-state, (2) Outer surface of annulus is adiabatic, (3) Ideal gas with negligible viscous dissipation and pressure variation, (4) Fully-developed flow throughout the tube, (5) Smooth tube surface, (6) Constant properties.

PROPERTIES: Table A-4, air ($\bar{T}_m \approx 325$ K, $p = 5$ atm): $\rho = 5 \times \rho(1 \text{ atm}) = 5.391 \text{ kg/m}^3$,

$c_p = 1008 \text{ J/kg} \cdot \text{K}$, $\mu = 196.4 \times 10^{-7} \text{ N} \cdot \text{s/m}^2$, $k = 0.0281 \text{ W/m} \cdot \text{K}$, $\text{Pr} = 0.703$. Table A-6, sat. steam ($p = 2.455$ bars): $T_s = 400$ K, $h_{fg} = 2183 \text{ kJ/kg}$.

ANALYSIS: With a uniform surface temperature, the air outlet temperature is

$$T_{m,o} = T_s - (T_s - T_{m,i}) \exp\left(-\frac{\pi D_i L \bar{h}}{\dot{m} c_p}\right)$$

With $\text{Re}_D = 4\dot{m}/\pi D_i \mu = 0.12 \text{ kg/s} / \pi (0.05 \text{ m}) 196.4 \times 10^{-7} \text{ kg/s} \cdot \text{m} = 38,980$, the flow is turbulent, and the Dittus-Boelter correlation yields

$$\bar{h} \approx h_{fd} = \left(\frac{k}{D_i}\right) 0.023 \text{Re}_D^{4/5} \text{Pr}^{0.4} = \left(\frac{0.0281 \text{ W/m} \cdot \text{K}}{0.05 \text{ m}}\right) 0.023 (38,980)^{4/5} (0.703)^{0.4} = 52.8 \text{ W/m}^2 \cdot \text{K}$$

$$T_{m,o} = 127^\circ\text{C} - (110^\circ\text{C}) \exp\left(-\frac{\pi \times 0.05 \text{ m} \times 5 \text{ m} \times 52.8 \text{ W/m}^2 \cdot \text{K}}{0.03 \text{ kg/s} \times 1008 \text{ J/kg} \cdot \text{K}}\right) = 99^\circ\text{C} \quad <$$

The pressure drop is $\Delta p = f \left(\rho u_m^2 / 2 D_i\right) L$, where, with $A_c = \pi D_i^2 / 4 = 1.963 \times 10^{-3} \text{ m}^2$, $u_m = \dot{m} / \rho A_c = 2.83 \text{ m/s}$, and with $\text{Re}_D = 38,980$, Eq. 8.21 gives $f = [0.790 \ln(\text{Re}_D) - 1.64]^{-2} = 0.022$. Hence,

$$\Delta p = 0.022 \times 5.391 \text{ kg/m}^3 \frac{(2.83 \text{ m/s})^2 5 \text{ m}}{2 \times 0.05 \text{ m}} = 47.5 \text{ N/m}^2 = 4.7 \times 10^{-4} \text{ atm} \quad <$$

The rate of heat transfer to the air is

$$q = \dot{m} c_p (T_{m,o} - T_{m,i}) = 0.03 \text{ kg/s} \times 1008 \text{ J/kg} \cdot \text{K} (82^\circ\text{C}) = 2480 \text{ W}$$

and the rate of condensation is then

$$\dot{m}_c = \frac{q}{h_{fg}} = \frac{2480 \text{ W}}{2.183 \times 10^6 \text{ J/kg}} = 1.14 \times 10^{-3} \text{ kg/s} \quad <$$

COMMENTS: (1) With $\bar{T}_m = (T_{m,i} + T_{m,o}) / 2 = 331 \text{ K}$, the initial estimate of 325 K is reasonable and iteration is not necessary. (2) For a steam flow rate of 0.01 kg/s, approximately 10% of the outflow would be in the form of saturated liquid, (3) With $L/D_i = 100$, it is reasonable to assume fully developed flow throughout the tube.