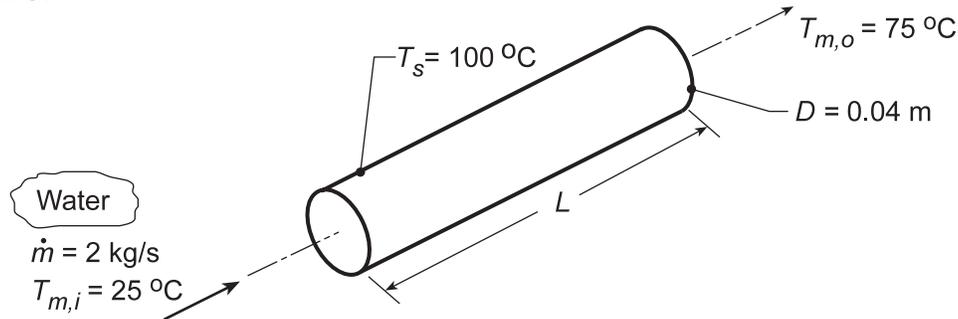


PROBLEM 8.35

KNOWN: Flow rate, inlet temperature and desired outlet temperature of water passing through a tube of prescribed diameter and surface temperature.

FIND: (a) Required tube length, L , for prescribed conditions, (b) Required length using tube diameters over the range $30 \leq D \leq 50$ mm with flow rates $\dot{m} = 1, 2$ and 3 kg/s; represent this design information graphically, and (c) Pressure gradient as a function of tube diameter for the three flow rates assuming the tube wall is smooth.

SCHEMATIC:



ASSUMPTIONS: (1) Steady-state conditions, (2) Incompressible liquid with negligible viscous dissipation, (3) Constant properties.

PROPERTIES: Table A.6, Water ($\bar{T}_m = 323$ K): $c_p = 4181$ J/kg·K, $\mu = 547 \times 10^{-6}$ N·s/m², $k = 0.643$ W/m·K, $Pr = 3.56$.

ANALYSIS: (a) From Eq. 8.6, the Reynolds number is

$$Re_D = \frac{4\dot{m}}{\pi D \mu} = \frac{4 \times 2 \text{ kg/s}}{\pi (0.04 \text{ m}) 547 \times 10^{-6} \text{ N} \cdot \text{s/m}^2} = 1.16 \times 10^5. \quad (1)$$

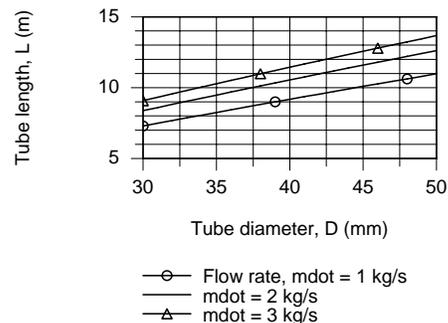
Hence the flow is turbulent, and assuming fully developed conditions throughout the tube, it follows from the Dittus-Boelter correlation, Eq. 8.60,

$$\bar{h} = \frac{k}{D} 0.023 Re_D^{4/5} Pr^{0.4} = \frac{0.643 \text{ W/m} \cdot \text{K}}{0.04 \text{ m}} 0.023 (1.16 \times 10^5)^{4/5} (3.56)^{0.4} = 6919 \text{ W/m}^2 \cdot \text{K} \quad (2)$$

From Eq. 8.41a, we then obtain

$$L = \frac{-\dot{m} c_p \ln(\Delta T_o / \Delta T_i)}{\pi D \bar{h}} = - \frac{2 \text{ kg/s} (4181 \text{ J/kg} \cdot \text{K}) \ln(25^\circ \text{C} / 75^\circ \text{C})}{\pi (0.04 \text{ m}) 6919 \text{ W/m}^2 \cdot \text{K}} = 10.6 \text{ m}. \quad \leftarrow$$

(b) Using the *IHT Correlations Tool, Internal Flow*, for fully developed *Turbulent Flow*, along with appropriate energy balance and rate equations, the required length L as a function of flow rate is computed and plotted on the right.



Continued...

PROBLEM 8.35 (Cont.)

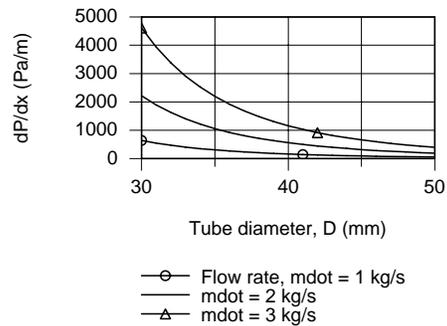
(c) From Eq. 8.22a the pressure drop is

$$\frac{\Delta p}{\Delta x} = f \frac{\rho u_m^2}{2D} \quad (4)$$

The friction factor, f , for the smooth surface condition, Eq. 8.21 with $3000 \leq Re_D \leq 5 \times 10^6$, is

$$f = (0.790 \ln(Re_D) - 1.64)^{-2} \quad (5)$$

Using IHT with these equations and Eq. (1), the pressure gradient as a function of diameter for the selected flow rates is computed and plotted on the right.



COMMENTS: (1) Since $L/D = (10.6/0.040) = 265$, the assumption of fully developed conditions throughout is justified.

(2) The IHT Workspace used to generate the graphical results are shown below.

```

// Rate Equation Tool - Tube Flow with Constant Surface Temperature:
/* For flow through a tube with a uniform wall temperature, Fig 8.7b, the
overall energy balance and heat rate equations are */
q = mdot*cp*(Tmo - Tmi) // Heat rate, W; Eq 8.34
(Ts - Tmo) / (Ts - Tmi) = exp ( - P * L * hDbar / (mdot * cp) ) // Eq 8.41b
// where the fluid and constant tube wall temperatures are
Ts = 100 + 273 // Tube wall temperature, K
Tmi = 25 + 273 // Inlet mean fluid temperature, K
Tmo = 75 + 273 // Outlet mean fluid temperature, K
// The tube parameters are
P = pi * D // Perimeter, m
Ac = pi * (D^2) / 4 // Cross sectional area, m^2
D = 0.040 // Tube diameter, m
D_mm = D * 1000
// The tube mass flow rate and fluid thermophysical properties are
mdot = rho * um * Ac
mdot = 1 // Mass flow rate, kg/s

// Correlation Tool - Internal Flow, Fully Developed Turbulent Flow (Assumed):
NuDbar = NuD_bar_IF_T_FD(ReD,Pr,n) // Eq 8.60
n = 0.4 // n = 0.4 or 0.3 for Ts>Tm or Ts<Tm
NuDbar = hDbar * D / k
ReD = um * D / nu
/* Evaluate properties at the fluid average mean temperature, Tmbar. */
Tmbar = Tfluid_avg (Tmi,Tmo)

// Properties Tool - Water:
// Water property functions :T dependence, From Table A.6
// Units: T(K), p(bars);
x = 0 // Quality (0=sat liquid or 1=sat vapor)
rho = rho_Tx("Water",Tmbar,x) // Density, kg/m^3
cp = cp_Tx("Water",Tmbar,x) // Specific heat, J/kg-K
nu = nu_Tx("Water",Tmbar,x) // Kinematic viscosity, m^2/s
k = k_Tx("Water",Tmbar,x) // Thermal conductivity, W/m-K
Pr = Pr_Tx("Water",Tmbar,x) // Prandtl number

// Pressure Gradient, Equations 8.21, 8.22a:
dPdx = f * rho * um^2 / ( 2 * D )
f = ( 0.790 * ln (ReD) - 1.64 ) ^ -2
    
```