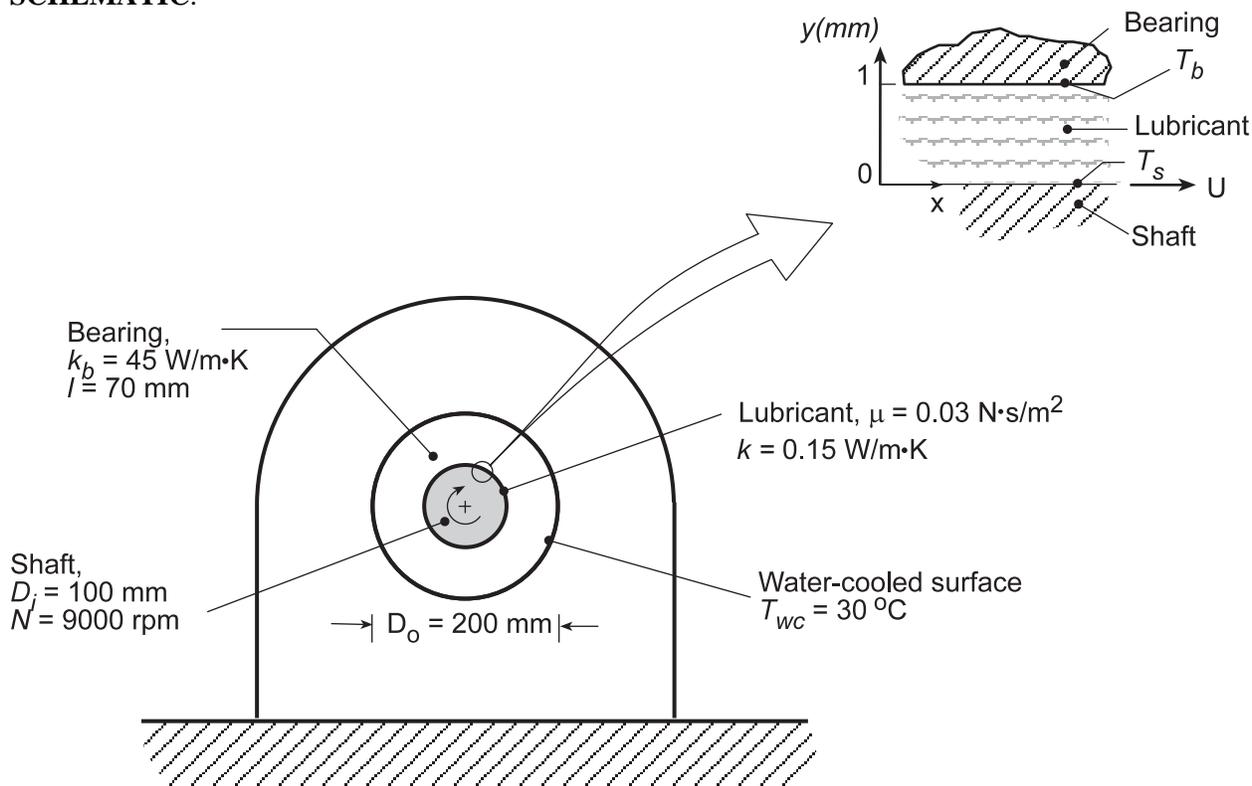


## PROBLEM 6S.8

**KNOWN:** Shaft of diameter 100 mm rotating at 9000 rpm in a journal bearing of 70 mm length. Uniform gap of 1 mm separates the shaft and bearing filled with lubricant. Outer surface of bearing is water-cooled and maintained at  $T_{wc} = 30^\circ\text{C}$ .

**FIND:** (a) Viscous dissipation in the lubricant,  $\mu\Phi(\text{W/m}^3)$ , (b) Heat transfer rate from the lubricant, assuming no heat lost through the shaft, and (c) Temperatures of the bearing and shaft,  $T_b$  and  $T_s$ .

**SCHEMATIC:**



**ASSUMPTIONS:** (1) Steady-state conditions, (2) Fully developed Couette flow, (3) Incompressible fluid with constant properties, and (4) Negligible heat lost through the shaft.

**ANALYSIS:** (a) The viscous dissipation,  $\mu\Phi$ , Eq. 6S.20, for Couette flow from Example 6S.1, is

$$\mu\Phi = \mu \left( \frac{du}{dy} \right)^2 = \mu \left( \frac{U}{L} \right)^2 = 0.03 \text{ N}\cdot\text{s/m}^2 \left( \frac{47.1 \text{ m/s}}{0.001 \text{ m}} \right)^2 = 6.656 \times 10^7 \text{ W/m}^3 \quad <$$

where the velocity distribution is linear and the tangential velocity of the shaft is

$$U = \pi DN = \pi (0.100 \text{ m}) \times 9000 \text{ rpm} \times (\text{min}/60\text{s}) = 47.1 \text{ m/s}.$$

(b) The heat transfer rate from the lubricant volume  $\forall$  through the bearing is

$$q = \mu\Phi \cdot \forall = \mu\Phi (\pi D \cdot L \cdot \ell) = 6.65 \times 10^7 \text{ W/m}^3 (\pi \times 0.100 \text{ m} \times 0.001 \text{ m} \times 0.070 \text{ m}) = 1462 \text{ W} \quad <$$

where  $\ell = 70 \text{ mm}$  is the length of the bearing normal to the page.

Continued...

### PROBLEM 6S.8 (Cont.)

(c) From Fourier's law, the heat rate through the bearing material of inner and outer diameters,  $D_i$  and  $D_o$ , and thermal conductivity  $k_b$  is, from Eq. (3.32),

$$q_r = \frac{2\pi\ell k_b (T_b - T_{wc})}{\ln(D_o/D_i)}$$

$$T_b = T_{wc} + \frac{q_r \ln(D_o/D_i)}{2\pi\ell k_b}$$

$$T_b = 30^\circ\text{C} + \frac{1462\text{ W} \ln(200/100)}{2\pi \times 0.070\text{ m} \times 45\text{ W/m}\cdot\text{K}} = 81.2^\circ\text{C} \quad <$$

To determine the temperature of the shaft,  $T(0) = T_s$ , first the temperature distribution must be found beginning with the general solution, Example 6S.1,

$$T(y) = -\frac{\mu}{2k} \left(\frac{U}{L}\right)^2 y^2 + C_3 y + C_4$$

The boundary conditions are, at  $y = 0$ , the surface is adiabatic

$$\left. \frac{dT}{dy} \right|_{y=0} = 0 \quad C_3 = 0$$

and at  $y = L$ , the temperature is that of the bearing,  $T_b$

$$T(L) = T_b = -\frac{\mu}{2k} \left(\frac{U}{L}\right)^2 L^2 + 0 + C_4 \quad C_4 = T_b + \frac{\mu}{2k} U^2$$

Hence, the temperature distribution is

$$T(y) = T_b + \frac{\mu}{2k} U^2 \left(1 - \frac{y^2}{L^2}\right)$$

and the temperature at the shaft,  $y = 0$ , is

$$T_s = T(0) = T_b + \frac{\mu}{2k} U^2 = 81.3^\circ\text{C} + \frac{0.03\text{ N}\cdot\text{s/m}^2}{2 \times 0.15\text{ W/m}\cdot\text{K}} (47.1\text{ m/s})^2 = 303^\circ\text{C} \quad <$$