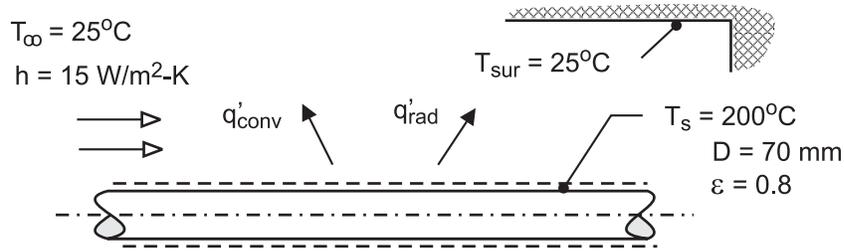


## PROBLEM 1.80

**KNOWN:** Uninsulated pipe of prescribed diameter, emissivity, and surface temperature in a room with fixed wall and air temperatures. See Example 1.2.

**FIND:** (a) Which option to reduce heat loss to the room is more effective: reduce by a factor of two the convection coefficient (from 15 to 7.5 W/m<sup>2</sup>·K) or the emissivity (from 0.8 to 0.4) and (b) Show graphically the heat loss as a function of the convection coefficient for the range 5 ≤ h ≤ 20 W/m<sup>2</sup>·K for emissivities of 0.2, 0.4 and 0.8. Comment on the relative efficacy of reducing heat losses associated with the convection and radiation processes.

**SCHEMATIC:**



**ASSUMPTIONS:** (1) Steady-state conditions, (2) Radiation exchange between pipe and the room is between a small surface in a much larger enclosure, (3) The surface emissivity and absorptivity are equal, and (4) Restriction of the air flow does not alter the radiation exchange process between the pipe and the room.

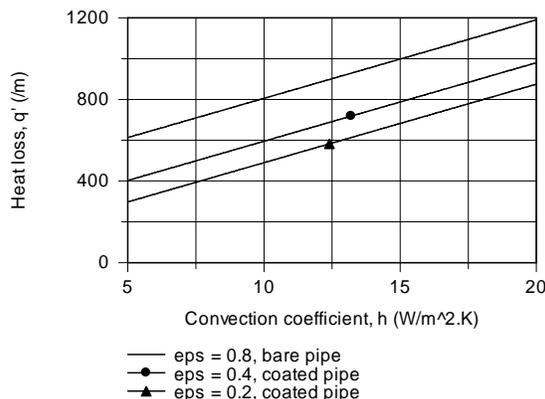
**ANALYSIS:** (a) The heat rate from the pipe to the room per unit length is

$$q' = q'/L = q'_{\text{conv}} + q'_{\text{rad}} = h(\pi D)(T_s - T_\infty) + \varepsilon(\pi D)\sigma(T_s^4 - T_{\text{sur}}^4)$$

Substituting numerical values for the two options, the resulting heat rates are calculated and compared with those for the conditions of Example 1.2. We conclude that both options are comparably effective.

Conditions	$h$ (W/m <sup>2</sup> ·K)	$\varepsilon$	$q'$ (W/m)
Base case, Example 1.2	15	0.8	998
Reducing $h$ by factor of 2	7.5	0.8	788
Reducing $\varepsilon$ by factor of 2	15	0.4	709

(b) Using IHT, the heat loss can be calculated as a function of the convection coefficient for selected values of the surface emissivity.



Continued ...

## PROBLEM 1.80 (Cont.)

**COMMENTS:** (1) In Example 1.2, Comment 3, we read that the heat rates by convection and radiation exchange were comparable for the base case conditions (577 vs. 421 W/m). It follows that reducing the key transport parameter ( $h$  or  $\epsilon$ ) by a factor of two yields comparable reductions in the heat loss. Coating the pipe to reduce the emissivity might be the more practical option as it may be difficult to control air movement.

(2) For this pipe size and thermal conditions ( $T_s$  and  $T_\infty$ ), the minimum possible convection coefficient is approximately  $7.5 \text{ W/m}^2 \cdot \text{K}$ , corresponding to free convection heat transfer to quiescent ambient air. Larger values of  $h$  are a consequence of forced air flow conditions.

(3) The Workspace for the IHT program to calculate the heat loss and generate the graph for the heat loss as a function of the convection coefficient for selected emissivities is shown below. It is good practice to provide commentary with the code making your solution logic clear, and to summarize the results.

```
// Heat loss per unit pipe length; rate equation from Ex. 1.2
q' = q'cv + q'rad
q'cv = pi*D*h*(Ts - Tinf)
q'rad = pi*D*eps*sigma*(Ts^4 - Tsur^4)
sigma = 5.67e-8

// Input parameters
D = 0.07
Ts_C = 200 // Representing temperatures in Celsius units using _C subscripting
Ts = Ts_C + 273
Tinf_C = 25
Tinf = Tinf_C + 273
h = 15 // For graph, sweep over range from 5 to 20
Tsur_C = 25
Tsur = Tsur_C + 273
eps = 0.8
//eps = 0.4 // Values of emissivity for parameter study
//eps = 0.2

/* Base case results
Tinf Ts Tsur q' q'cv q'rad D Tinf_C Ts_C Tsur_C
eps h sigma
298 473 298 997.9 577.3 420.6 0.07 25 200 25
0.8 15 5.67E-8 */
```